

UNIT – III

Finite Impulse Response (FIR)

Filter Design: Rectangular, Triangular, Hamming, Blackman & Kaiser window.

Linear Phase and Optimal Filter.

FIR FILTER

An FIR filter of length M is described by the difference equation

$$y(n) = b_0 x(n) + b_1 x(n - 1) + b_2 x(n - 2) + b_3 x(n - 3) + \dots \\ + b_{M-1} x(n - M + 1)$$

$$= \sum_{k=0}^{M-1} b_k x(n - k)$$

where b_k is the set of filter coefficients.

THE response of the FIR filter depends only on the present and past t samples, whereas for the IIR filter, the present response is a function of the present and past N values of excitation as well as past values of the response.

FIR filters have the following advantages over IIR filters

- (i) They can have an exact linear phase.
- (ii) They are always stable.
- (iii) The design methods are generally linear.
- (iv) They can be realised efficiently in hardware.
- (v) The filter start-up transients have finite duration.

MAGNITUDE RESPONSE AND PHASE RESPONSE OF DIGITAL FILTERS

The discrete-time Fourier transform of a finite sequence impulse response $h(n)$ is given by

$$H(e^{j\omega}) = \sum_{n=0}^{M-1} h(n)e^{-j\omega nT} = |H(e^{j\omega})| e^{j\Phi(\omega)}$$

The magnitude and phase responses are given by

$$M(\omega) = |H(e^{j\omega})| = \{\text{Re}[H(e^{j\omega})]^2 + \text{Im}[H(e^{j\omega})]^2\}^{0.5}$$

$$\Phi(\omega) = \tan^{-1} \frac{\text{Im}[H(e^{j\omega})]}{\text{Re}[H(e^{j\omega})]}$$

Filters can have a linear or non-linear phase depending upon the delay function, namely the phase delay and group delay. The phase and group delays of the filter are given by

$$\tau_p = -\frac{\Phi(\omega)}{\omega} \quad \text{and} \quad \tau_g = -\frac{d\Phi(\omega)}{d\omega}, \quad \text{respectively.}$$

LINEAR PHASE FILTER ARE THOSE FILTERS IN WHICH THE PHASE DELAY AND GROUP DELAY ARE CONSTANTS, i.e. INDEPENDENT OF FREQUENCY. (time delay filters)

For the phase response to be linear

$$\frac{\Phi(\omega)}{\omega} = -\tau, \quad -\pi \leq \omega \leq +\pi$$

$$\Phi(\omega) = \tan^{-1} \frac{\text{Im } H(e^{j\omega})}{\text{Re } H(e^{j\omega})} = -\omega\tau$$

$$h(n) = -h(M-1-n)$$

or

$$\tan \omega \tau = \frac{\sum_{n=0}^{M-1} h(n) \sin \omega n}{\sum_{n=0}^{M-1} h(n) \cos \omega n}$$

Simplifying, we get

$$\sum_{n=0}^{M-1} h(n) \sin (\omega \tau - \omega n) = 0$$

and a solution τ is given by

$$\tau = \frac{(M-1)}{2}$$

and

$$h(n) = h(M-1-n) \text{ for } 0 < n < M-1$$

Example 7.1 The length of an FIR filter is 9. If the filter has a linear phase, show that below is satisfied.

$$\sum_{n=0}^{M-1} h(n) \sin(\omega \tau - \omega n) = 0$$

Example 7.2 The following transfer function characterises an FIR filter ($M = 11$). Determine the magnitude response and show that the phase and group delays are constant.

$$H(z) = \sum_{n=0}^{M-1} h(n) z^{-n}$$

Solution The length of the filter, $M = 9$. Therefore, from

$$\tau = \frac{(M-1)}{2} = 4.$$

$h(n) = h(M-1-n)$. Therefore the filter coefficients are $h(0) = h(8)$, $h(1) = h(7)$, $h(2) = h(6)$, $h(3) = h(5)$ and $h(4)$.

Eq. 7.3 can be written as,

$$\begin{aligned} \sum_{n=0}^{M-1} h(n) \sin(\omega\tau - \omega n) &= \sum_{n=0}^8 h(n) \sin \omega(\tau - n) \\ &= h(0) \sin 4\omega + h(1) \sin 3\omega + h(2) \sin 2\omega + h(3) \sin \omega + h(4) \sin 0 \\ &\quad + h(5) \sin(-\omega) + h(6) \sin(-2\omega) + h(7) \sin(-3\omega) + h(8) \sin(-4\omega) \\ &= 0 \end{aligned}$$

Thus Eq above is satisfied.

Solution The transfer function of the filter is given by

$$\begin{aligned} H(z) &= \sum_{n=0}^{M-1} h(n) z^{-n} \\ &= h(0) + h(1) z^{-1} + h(2) z^{-2} + \dots + h(10) z^{-10} \end{aligned}$$

The phase delay, $\tau = \frac{M-1}{2} = 5$. Since $\tau = 5$, the transfer function can be expressed as,

$$H(z) = z^{-5} [h(0) z^5 + h(1) z^4 + h(2) z^3 + \dots + h(9) z^{-4} + h(10) z^{-5}]$$

Since $h(n) = h(M - 1 - n)$,

$$H(z) = z^{-5} [h(0)(z^5 + z^{-5}) + h(1)(z^4 + z^{-4}) + h(2)(z^3 + z^{-3}) \\ + h(3)(z^2 + z^{-2}) + h(4)(z + z^{-1}) + h(5)]$$

The frequency response is obtained by replacing z with $e^{j\omega}$,

$$H(e^{j\omega}) = e^{-j5\omega} \{h(0)[e^{5j\omega} + e^{-5j\omega}] + h(1)[e^{4j\omega} + e^{-4j\omega}] \\ + h(2)[e^{3j\omega} + e^{-3j\omega}] + h(3)[e^{2j\omega} + e^{-2j\omega}] \\ + h(4)[e^{j\omega} + e^{-j\omega}] + h(5)\} \\ = e^{-j5\omega} \left[h(5) + 2 \sum_{n=0}^4 h(n) \cos(\tau - n)\omega \right] = e^{-j5\omega} M(\omega)$$

where $M(\omega)$ is the magnitude response and $\theta(\omega) = -5\omega$ is the phase response. The group delay, τ_g is given by,

$$\tau_p = -\frac{\Phi(\omega)}{\omega} = 5 \quad \text{and} \quad \tau_g = -\frac{d[\Phi(\omega)]}{d\omega} = -\frac{d(-5\omega)}{d\omega} = 5$$

Thus, the phase delay and the group delay are the same and are constants.

FREQUENCY RESPONSE OF LINEAR PHASE FIR FILTERS

$$H(e^{j\omega}) = e^{-j\omega\left(\frac{M-1}{2}\right)T} \left\{ \sum_{k=0}^{\frac{M-1}{2}} a(k) \cos \omega kT \right\}$$

$$= e^{-j\omega\left(\frac{M-1}{2}\right)T} = M(\omega)$$

DESIGN TECHNIQUES FOR FIR FILTERS

.1 **Fourier Series Method**

.2 **Frequency Sampling Method**

.3 **Window Techniques**

Window Techniques

The desired frequency response of any digital filter is

$$H_d(e^{j\omega}) = \sum_{n=-\infty}^{\infty} h_d(n) e^{-j\omega n} \quad \text{where:} \quad h(n) = \frac{1}{2\pi} \int_0^{2\pi} H(e^{j\omega}) e^{j\omega n} d\omega$$

The Fourier transform of the window function $W(e^{j\omega})$ should have a small width of main lobe containing as much of the total energy as possible.

The Fourier transform of the window function $W(e^{j\omega})$ should have side lobes that decrease in energy rapidly as ω tends to π . Some of the most frequently used window functions are described in the following sections.

The Fourier coefficients of the series $h(n)$ are identical to the impulse response of a digital filter. There are two difficulties with implementation of equation

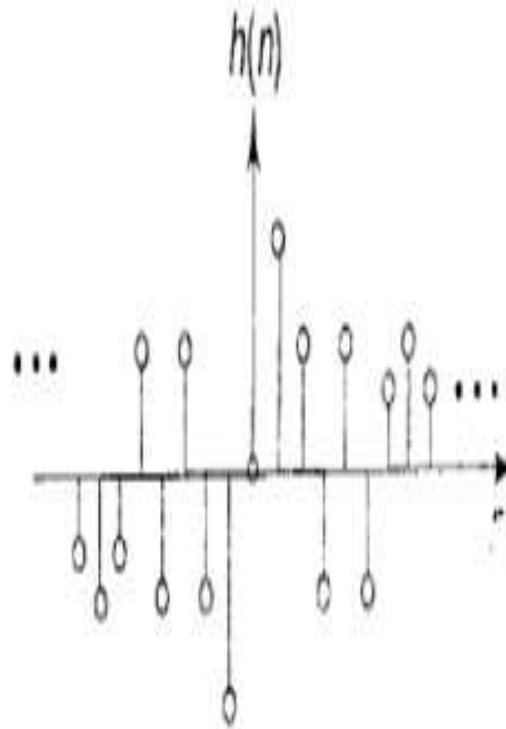
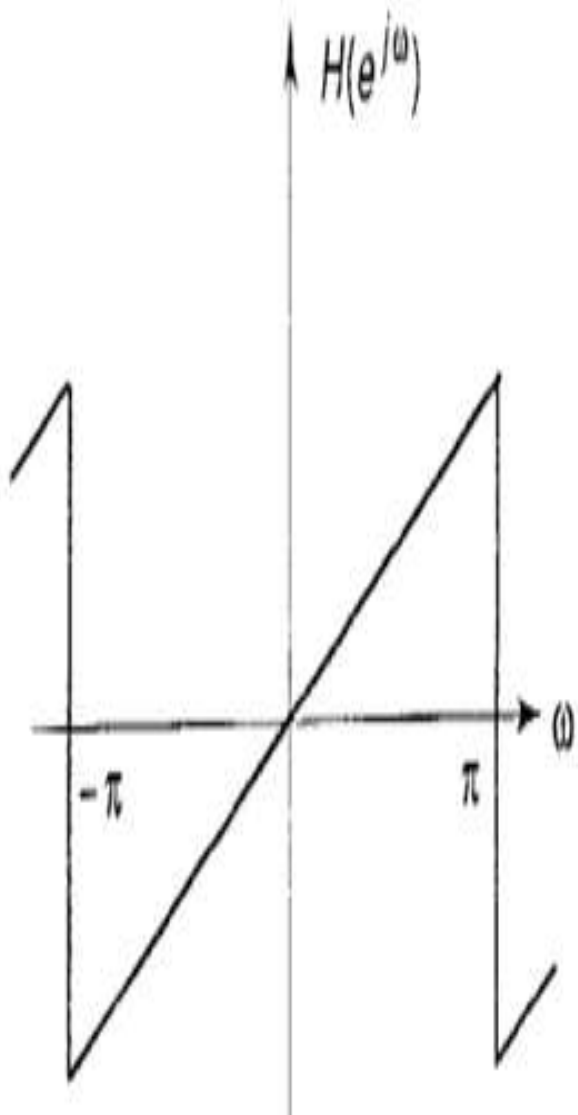
$$H_d(e^{j\omega}) = \sum_{n=-\infty}^{\infty} h_d(n) e^{-j\omega n} \text{ for designing a digital filter.}$$

1) Impulse response is of infinite duration.

2) The filter is noncausal and unrealizable. So $H(e^{j\omega})$ is an unrealisable IIR filter.

Solution of above is to convert infinite duration impulse response to finite duration by truncating the infinite series at $n=\pm N$ but result in undesirable oscillations in passband and stopband of the digital filter.

These undesirable oscillations can be reduced by using a set of time-limited weighting function, $w(n)$, referred to as WINDOW FUNCTIONS, to modify the Fourier coefficients.



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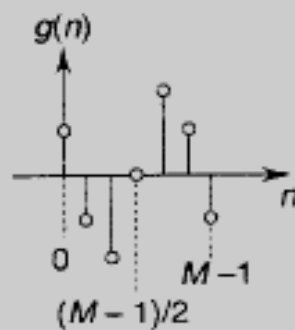
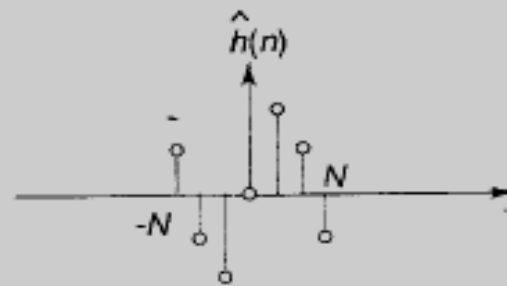
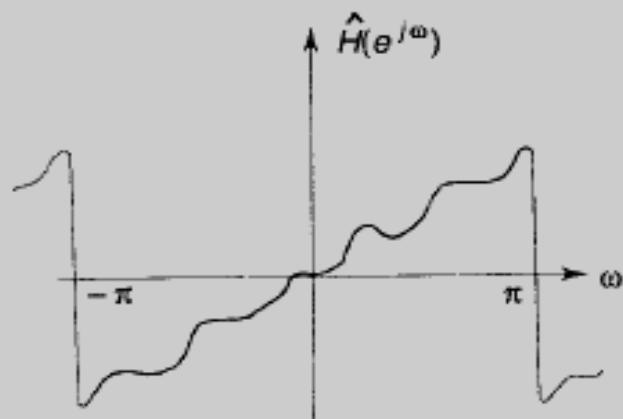
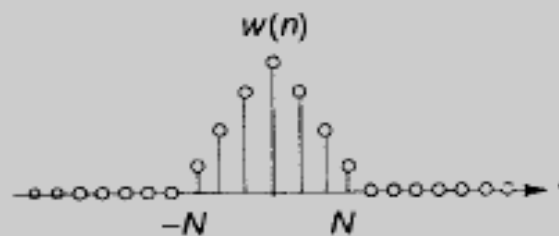
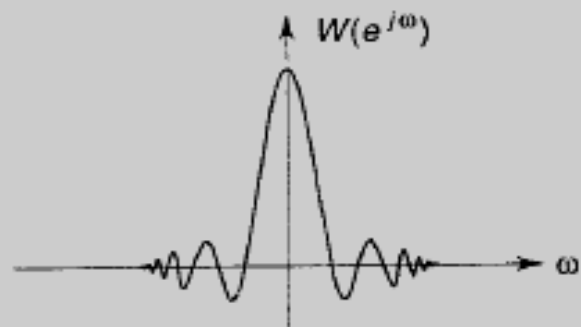
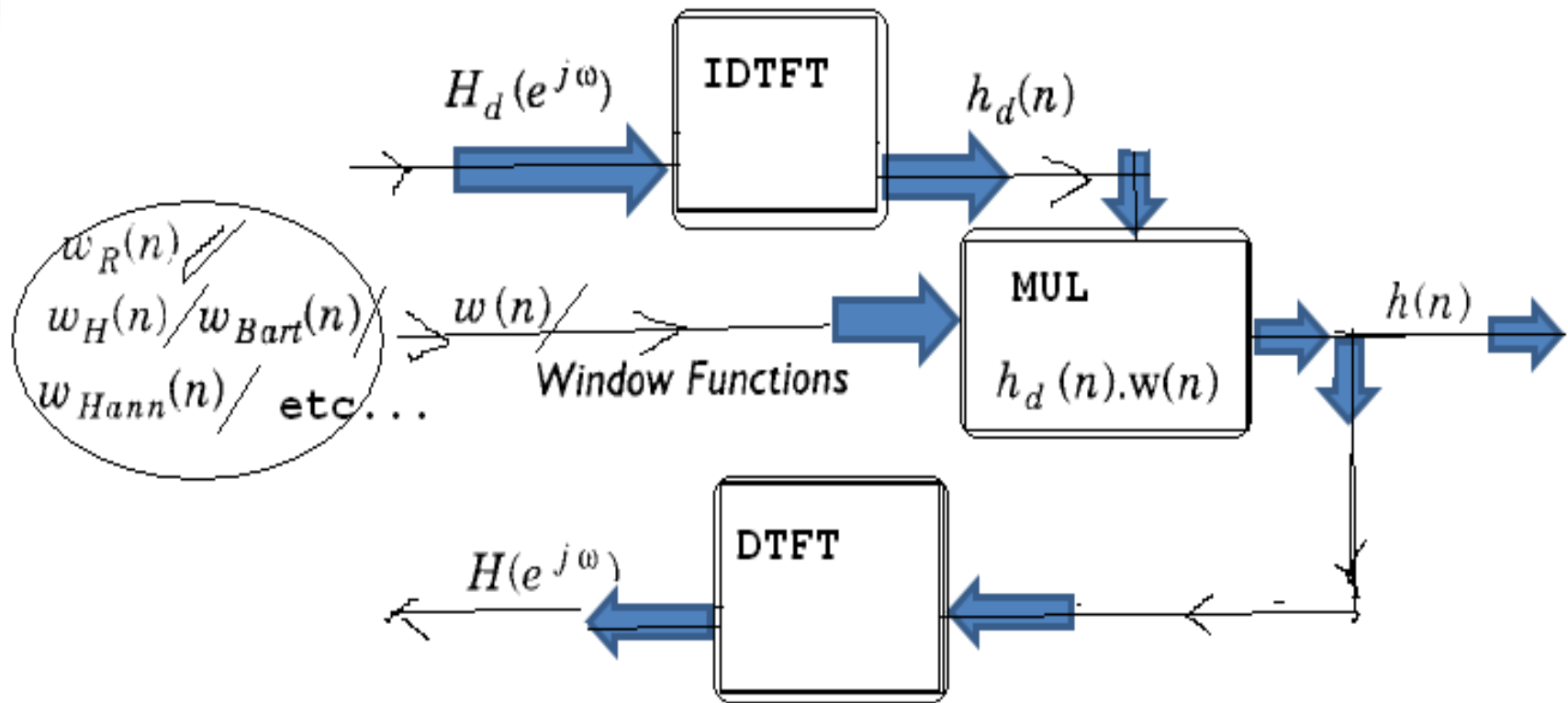


Illustration of the Window Technique

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FLOW DIAGRAM FOR DESIGN FIR FILTER USING WINDOW METHOD



frequency response of the designed low-pass filter is $H(e^{j\omega})$

filter coefficients of the filter $h(n) = h_d(n) \cdot w(n)$

window function $w(n)$

desired frequency response $H_d(e^{j\omega})$

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TYPES OF WINDOW FUNCTION:

1. RECTANGULAR WINDOW FUNCTION.
2. HAMMING WINDOW FUNCTION.
3. *HANNING WINDOW FUNTION.*
4. BLACKMAN WINDOW FUNCTION.
5. *BARTLET WINDOW FUNCTION.*
6. TRINGULAR WINDOW FUNTION.
7. KAISER WINDOW
8. _etc...

Kaiser window.

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Rectangular Window Function

The weighting function for the rectangular window is given by

$$w_R(n) = \begin{cases} 1, & \text{for } |n| \leq \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$

$$W_R(e^{j\omega T}) = \frac{\sin\left(\frac{\omega M T}{2}\right)}{\sin\left(\frac{\omega T}{2}\right)}$$

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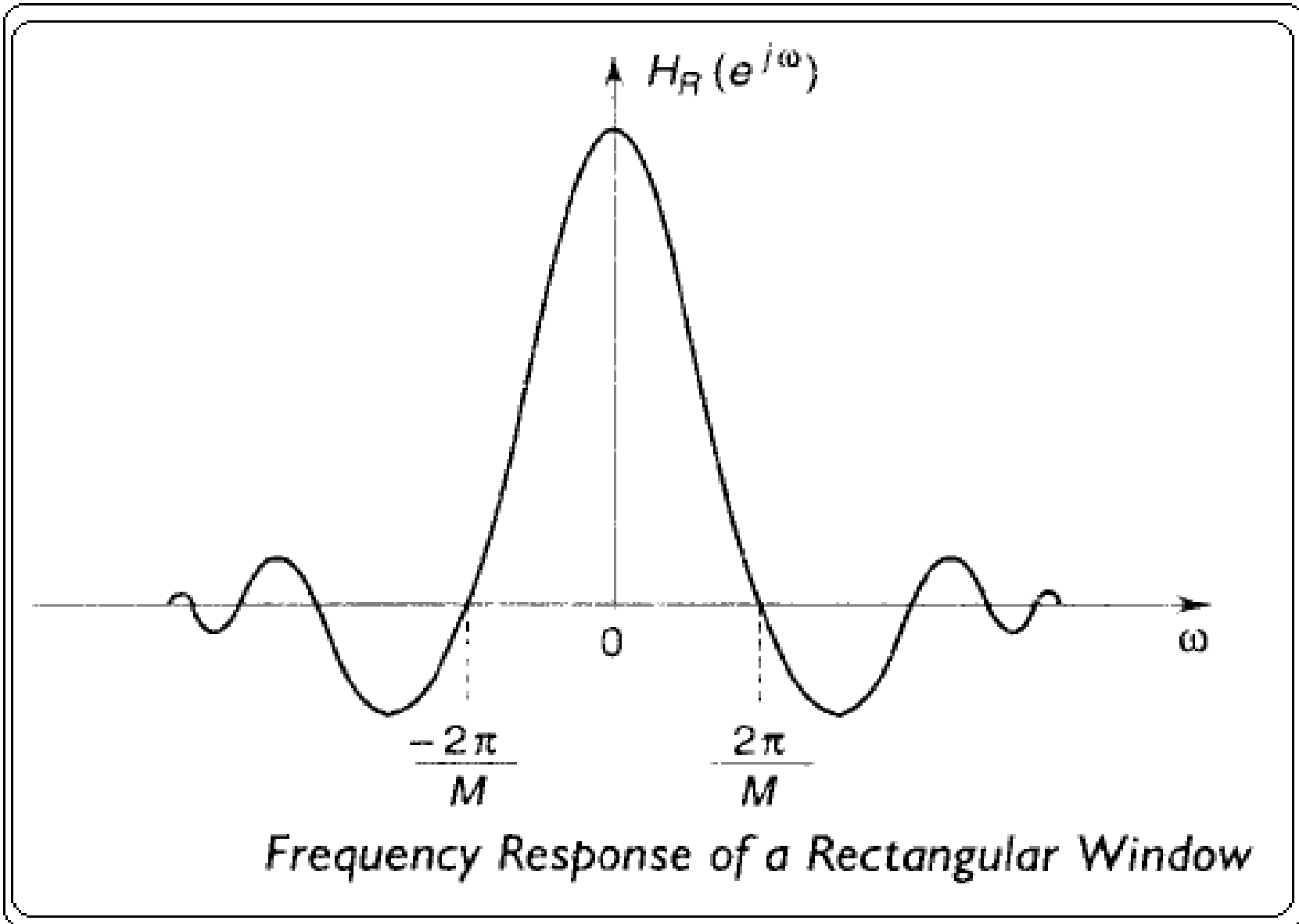
Hamming Window Function

causal Hamming window function is expressed by

$$w_H(n) = \begin{cases} 0.54 - 0.46 \cos \frac{2\pi n}{M-1}, & 0 \leq n < M-1 \\ 0, & \text{otherwise} \end{cases}$$

non-causal Hamming window function is given by

$$w_H(n) = \begin{cases} 0.54 + 0.46 \cos \frac{2\pi n}{M-1}, & \text{for } |n| \leq \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$



Frequency Response of a Rectangular Window

003. **Blackman Window Function**

· window function of a **causal** Blackman window is expressed by

$$W_{\text{black}}(n) = \begin{cases} 0.42 - 0.5 \cos \frac{2\pi n}{M-1} + 0.08 \cos \frac{4\pi n}{M-1}, & 0 \leq n \leq M-1 \\ 0, & \text{otherwise} \end{cases}$$

· window function of a **non-causal** Blackman window is given by

$$W_{\text{black}}(n) = \begin{cases} 0.42 + 0.5 \cos \frac{2\pi n}{M-1} + 0.08 \cos \frac{4\pi n}{M-1}, & \text{for } |n| < \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$

· main lobe is approximately $12\pi/M$; side-lobe is at -58dB .

004 BARTLETT TRIANGULAR WINDOW

window function of a non-causal Bartlett window is expressed by

$$w_{Bart}(n) = \begin{cases} 1+n, & -\frac{M-1}{2} < n < 1 \\ 1-n, & 1 < n < \frac{M-1}{2} \end{cases}$$

Frequency-Domain Characteristics of Some Window Functions

TYPES OF WINDOW--	<i>Approximate Transition Width of Main Lobe</i>	<i>Minimum Stopband Attenuation (dB)</i>	<i>Peak of first Sidelobe (dB)</i>
RECTANGULAR-----	$4\pi / M$	-21	-13
BARTLETT-----	$8\pi / M$	-25	-27
HANNING-----	$8\pi / M$	-44	-32
HAMMING-----	$8\pi / M$	-53	-43
BLACKMAN-----	$12\pi / M$	-74	-58

Example 7.5 A low-pass filter is to be designed with the following desired frequency response

$$H_d(e^{j\omega}) = \begin{cases} e^{-j2\omega}, & -\pi/4 \leq \omega \leq \pi/4 \\ 0, & \pi/4 < |\omega| \leq \pi \end{cases}$$

Determine the filter coefficients $h_d(n)$ if the window function is defined as

$$w(n) = \begin{cases} 1, & 0 \leq n \leq 4 \\ 0, & \text{otherwise} \end{cases}$$

Also, determine the frequency response $H(e^{j\omega})$ of the designed filter.

Example 7.5

Solution Given

$$H_d(e^{j\omega}) = \begin{cases} e^{-j2\omega}, & -\pi/4 \leq \omega \leq \pi/4 \\ 0, & \pi/4 < |\omega| \leq \pi \end{cases}$$

Therefore,

$$\begin{aligned} h_d(n) &= \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega \\ &= \frac{1}{2\pi} \int_{-\pi/4}^{\pi/4} e^{-j2\omega} e^{j\omega n} d\omega \\ &= \frac{1}{2\pi} \int_{-\pi/4}^{\pi/4} e^{j\omega(n-2)} d\omega \\ &= \frac{1}{\pi(n-2)} \left[\frac{e^{j(n-2)\pi/4} - e^{-j(n-2)\pi/4}}{2j} \right] \\ &= \frac{1}{\pi(n-2)} \sin \frac{\pi}{4}(n-2), \quad n \neq 2 \end{aligned}$$

For $n = 2$, the filter coefficient can be obtained by applying L'Hospital's rule to the above expression. Thus,

$$h_d(2) = \frac{1}{4}$$

The other filter coefficients are given by

$$h_d(0) = \frac{1}{2\pi} = h_d(4) \quad \text{and} \quad h_d(1) = \frac{1}{\sqrt{2}\pi} = h_d(3)$$

The filter coefficients of the filter would be then

$$h(n) = h_d(n) \cdot w(n)$$

Therefore,

$$h(0) = \frac{1}{2\pi} = h(4), \quad h(1) = \frac{1}{\sqrt{2}\pi} = h(3) \quad \text{and} \quad h(2) = \frac{1}{4}$$

The frequency response $H(e^{j\omega})$ is given by

$$H(e^{j\omega}) = \sum_{n=0}^4 h(n) e^{-j\omega n}$$

$$\begin{aligned} &= h(0) + h(1) e^{-j\omega} + h(2) e^{-j2\omega} + h(3) e^{-j3\omega} + h(4) e^{-j4\omega} \\ &= e^{-j2\omega} [h(0) e^{j2\omega} + h(1) e^{j\omega} + h(2) + h(3) e^{-j\omega} + h(4) e^{-j2\omega}] \\ &= e^{-j2\omega} \{h(2) + h(0) [e^{j2\omega} + e^{-j2\omega}] + h(1) [e^{j\omega} + e^{-j\omega}]\} \end{aligned}$$

$$= e^{-j2\omega} \left\{ \frac{1}{4} + \frac{1}{2\pi} [e^{j2\omega} + e^{-j2\omega}] + \frac{1}{\sqrt{2}\pi} [e^{j\omega} + e^{-j\omega}] \right\}$$

The frequency response of the designed low-pass filter is then,

$$H(e^{j\omega}) = e^{-j2\omega} \left\{ \frac{1}{4} + \frac{\sqrt{2}}{\pi} \cos \omega + \frac{1}{\pi} \cos 2\omega \right\}$$

Example 7.6 A filter is to be designed with the following desired frequency response

$$H_d(e^{j\omega}) = \begin{cases} 0, & -\pi/4 \leq \omega \leq \pi/4 \\ e^{-j2\omega}, & \pi/4 \leq |\omega| \leq \pi \end{cases}$$

Determine the filter coefficients $h_d(n)$ if the window function is defined as

$$w(n) = \begin{cases} 1, & 0 \leq n \leq 4 \\ 0, & \text{otherwise} \end{cases}$$

Also, determine the frequency response $H(e^{j\omega})$ of the designed filter.

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Example 7.6*Solution* Given

$$H_d(e^{j\omega}) = \begin{cases} 0, & -\pi/4 \leq \omega \leq \pi/4 \\ e^{-j2\omega}, & \pi/4 < |\omega| \leq \pi \end{cases}$$

Therefore,

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$

$$= \frac{1}{2\pi} \int_{-\pi}^{-\pi/4} e^{-j2\omega} e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{\pi/4}^{\pi} e^{-j2\omega} e^{j\omega n} d\omega$$

$$= \frac{1}{2\pi} \int_{-\pi}^{-\pi/4} e^{j\omega(n-2)} d\omega + \frac{1}{2\pi} \int_{\pi/4}^{\pi} e^{j\omega(n-2)} d\omega$$

$$= \frac{1}{\pi(n-2)} \left\{ \left[\frac{e^{j(n-2)\pi} - e^{-j(n-2)\pi}}{2j} \right] - \left[\frac{e^{j(n-2)\pi/4} - e^{-j(n-2)\pi/4}}{2j} \right] \right\}$$

7.6

Solution Given

$$= \frac{1}{\pi(n-2)} [\sin \pi(n-2) - \sin (n-2)\pi/4], \quad n \neq 2$$

The filter coefficients are given by,

$$h_d(2) = \frac{3}{4}, \quad h_d(0) = \frac{1}{2\pi} = h_d(4) \quad \text{and} \quad h_d(1) = \frac{1}{\sqrt{2}\pi} = h_d(3)$$

and by applying the window function, the new filter coefficients are

$$h(2) = \frac{3}{4}, \quad h(0) = \frac{1}{2\pi} = h(4) \quad \text{and} \quad h(1) = \frac{1}{\sqrt{2}\pi} = h(3)$$

The frequency response $H(e^{j\omega})$, is obtained as in the previous example,

$$H(e^{j\omega}) = e^{-j2\omega} \left[0.75 - \frac{\sqrt{2}}{\pi} \cos \omega - \frac{1}{\pi} \cos 2\omega \right]$$

Example 7.7 A low-pass filter should have the frequency response given below. Find the filter coefficients $h_d(n)$. Also determine τ so that $h_d(n) = h_d(-n)$.

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\tau}, & -\omega_c \leq \omega \leq \omega_c \\ 0, & \omega_c < |\omega| \leq \pi \end{cases}$$

Example 7.8 The desired response of a low-pass filter is

$$H_d(e^{j\omega}) = \begin{cases} e^{-j3\omega}, & -3\pi/4 \leq \omega \leq 3\pi/4 \\ 0, & 3\pi/4 < |\omega| \leq \pi \end{cases}$$

Determine $H(e^{j\omega})$ for $M = 7$ using a Hamming window.

Example 7.9 Design an FIR digital filter to approximate an ideal low-pass filter with passband gain of unity, cut-off frequency of 850 Hz and working at a sampling frequency of $f_s = 5000$ Hz. The length of the impulse response should be 5. Use a rectangular window.

Example 7.7

Solution The filter coefficients are given by

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{-j\omega\tau} e^{j\omega n} d\omega$$

$$h_d(n) = \frac{\sin \omega_c (n - \tau)}{\pi (n - \tau)}, \quad n \neq \tau \text{ and } h_d(\tau) = \frac{\omega_c}{\pi}$$

when $h_d(n) = h_d(-n)$,

$$\frac{\sin \omega_c (n - \tau)}{\pi (n - \tau)} = \frac{\sin \omega_c (-n - \tau)}{\pi (-n - \tau)}$$

That is,

$$\frac{\sin \omega_c (n - \tau)}{\pi (n - \tau)} = \frac{-\sin \omega_c (n + \tau)}{-\pi (n + \tau)} = \frac{\sin \omega_c (n + \tau)}{\pi (n + \tau)}$$

This is possible only when $(n - \tau) = (n + \tau)$ or $\tau = 0$.

Solution The filter coefficients are given by **Example 7.8**

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-3\pi/4}^{3\pi/4} e^{-j3\omega} e^{j\omega n} d\omega$$

$$h_d(n) = \frac{\sin 3\pi(n-3)/4}{\pi(n-3)}, \quad n \neq 3 \text{ and } h_d(3) = \frac{3}{4}$$

The filter coefficients are,

$$h_d(0) = 0.0750, h_d(1) = -0.1592, h_d(2) = 0.2251, h_d(3) = 0.75$$
$$h_d(4) = 0.2251, h_d(5) = -0.1592, h_d(6) = 0.0750$$

The Hamming window function is,

$$w(n) = \begin{cases} 0.54 - 0.46 \cos \frac{2\pi n}{M-1}, & 0 \leq n \leq M-1 \\ 0, & \text{otherwise} \end{cases}$$

Therefore, with $M = 7$,

$$w(0) = 0.08, w(1) = 0.31, w(2) = 0.77, w(3) = 1, w(4) = 0.77,$$
$$w(5) = 0.31, w(6) = 0.08.$$

The filter coefficients of the resultant filter are then,

$$h(n) = h_d(n).w(n) \quad n = 0, 1, 2, 3, 4, 5, 6. \quad \text{agk-RCET-BHILAI}$$

Therefore,

$$h(0) = 0.006, h(1) = -0.0494, h(2) = 0.1733, h(3) = 0.75,$$

$$h(4) = 0.1733, h(5) = -0.0494 \text{ and } h(6) = 0.006.$$

The frequency response is given by

$$H(e^{j\omega}) = \sum_{n=0}^6 h(n) e^{-j\omega n}$$

$$= e^{-j3\omega} [h(3) + 2h(0) \cos 3\omega + 2h(1) \cos 2\omega + 2h(2) \cos \omega]$$

$$= e^{-j3\omega} [0.75 + 0.3466 \cos \omega - 0.0988 \cos 2\omega + 0.012 \cos \omega]$$

Example 7.9

Solution The desired response of the ideal low-pass filter is given by

$$H_d(e^{j\omega}) = \begin{cases} 1, & 0 \leq f \leq 850 \text{ Hz} \\ 0, & f > 850 \text{ Hz} \end{cases}$$

The above response can be equivalently specified in terms of the normalised ω_c . The normalised $\omega_c = 2\pi f_c / f_s = 2\pi (850) / (5000) = 1.068$ rad/sec. Hence, the desired response is

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$

$$H_d(e^{j\omega}) = \begin{cases} 1, & 0 \leq |\omega| \leq 1.068 \\ 0, & 1.068 < |\omega| \leq \pi \end{cases}$$

The filter coefficients are given by

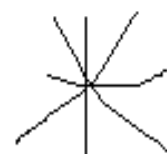
Therefore,

$$h(0) = 0.34, h(1) = 0.2789, h(2) = 0.1344, h(3) = -0.0066, \\ h(4) = -0.0720$$

$$h_d(n) = \frac{\sin 1.068 n}{\pi n}, \quad n \neq 0 \quad \text{and} \quad h_d(0) = \frac{1.068}{\pi} = 0.3400$$

Using the rectangular window function and for $M = 5$,

$$h(n) = h_d(n) \cdot w(n) \quad n = 0, 1, 2, 3, 4.$$



005. **Kaiser Window**

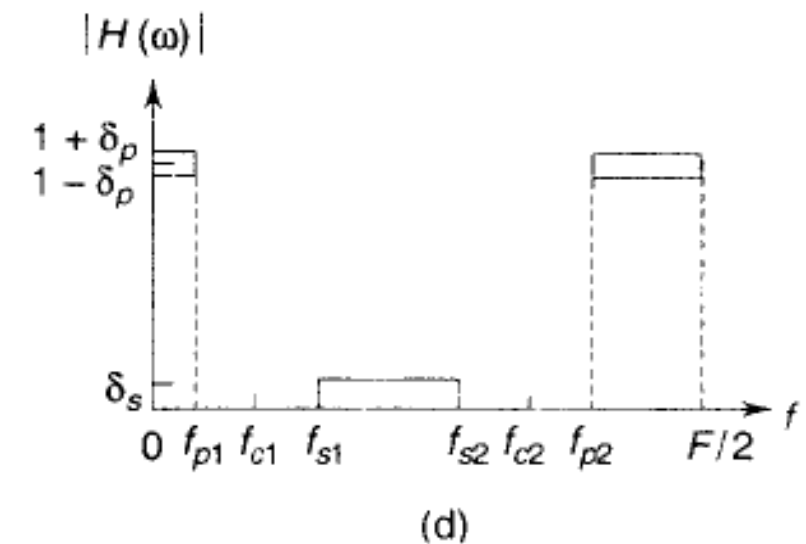
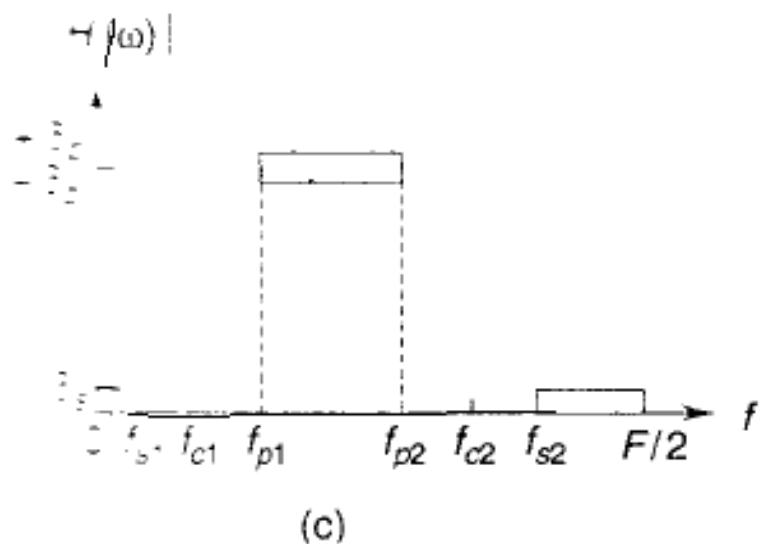
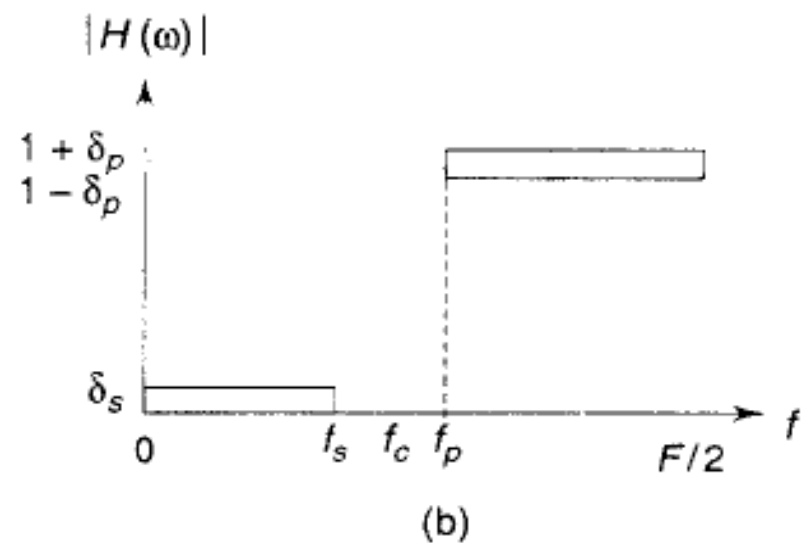
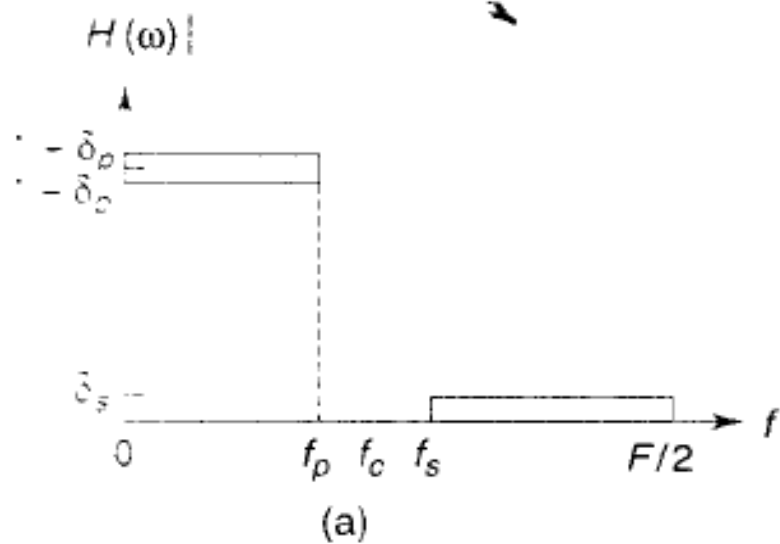
width of the main lobe ^{proportional to}
inversely proportional to the length of the filter.

Kaiser window, the side lobe level can be controlled with respect ^{adv over above} filter
mainlobe peak by varying a parameter, α .

The width of the main lobe ^{can}
can be varied by adjusting the length of the filter.

function is given by

$$w_K(n) = \begin{cases} \frac{I_0(\beta)}{I_0(\alpha)}, & \text{for } |n| \leq \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$



Idealised Frequency Responses: (a) low-pass filter; (b) high-pass filter; (c) bandpass filter; (d) bandstop filter

Design Using the Kaiser Window Function

Design Specifications

1. Filter type : Low-pass, high-pass, bandpass or bandstop.
2. Passband and stopband frequencies in hertz:
For low-pass / high-pass : f_p and f_s .
For band-pass / band-stop : f_{p1} , f_{p2} , f_{s1} and f_{s2} .
3. Passband ripple and minimum stopband attenuation in positive decibels: A'_p and A'_s .
4. Sampling frequency in hertz : F
5. Filter order M - odd.

agk-rcet-bhilai

OUR AIM TO DETERMINE:

$$h(n) = w_K(n) h_d(n),$$

DESIGN PROCEDURE FOR KAISER WINDOW:

Design Procedure

$$w_K(n) = \begin{cases} \frac{I_0(\beta)}{I_0(\alpha)}, & \text{for } |n| \leq \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$

$$I_0(x) = 1 + \sum_{k=1}^{\infty} \left[\frac{1}{k!} \left(\frac{x}{2} \right)^k \right]^2$$

WHERE:

$$\beta = \alpha \left[1 - \left(\frac{2n}{M-1} \right)^2 \right]^{0.5}$$

FIRST STEP:

The length of the filter, M :

$$M \geq \frac{FD}{\Delta F} + 1$$

$$D = \begin{cases} 0.9222, & \text{for } A_S \leq 21 \\ \frac{A_S - 7.95}{14.36}, & \text{for } A_S > 21 \end{cases}$$

The transition bandwidth is

$$\Delta F = f_S - f_P \quad \cdot \text{ Sampling frequency in hertz : } F$$

$$A_P = 20 \log_{10} \frac{1 + \delta_p}{1 - \delta_p} \text{ dB}$$

where A_P and A_S are the actual passband peak-to-peak ripple and minimum stopband attenuation, respectively.

$$A_S = -20 \log_{10} \delta_S \text{ dB} \quad \text{Suppose } M=23 \text{ so } |n|=-13 \text{ to } -1, \text{ then } 0 \text{ then } 1 \text{ to } 13$$

The filter coefficients of the non-causal digital filter $\{h(n) = h(-n)\}$

STEP SECOND:

$$w_K(n) = \begin{cases} \frac{I_0(\beta)}{I_0(\alpha)}, & \text{for } |n| \leq \frac{M-1}{2} \\ 0, & \text{otherwise} \end{cases}$$

WHERE:

$$\beta = \alpha \left[1 - \left(\frac{2n}{M-1} \right)^2 \right]^{0.5}$$

$$I_0(x) = 1 + \sum_{k=1}^{\infty} \left[\frac{1}{k!} \left(\frac{x}{2} \right)^k \right]^2$$
$$= 1 + \frac{0.25x^2}{(1!)^2} + \frac{(0.25x^2)^2}{(2!)^2} + \frac{(0.25x^2)^3}{(3!)^2} + \dots$$

Determine the parameter α from the Kaiser's design equation

$$\alpha = \begin{cases} 0, & \text{for } A_S \leq 21 \\ 0.5842(A_S - 21)^{0.4} + 0.07886(A_S - 21), & \text{for } 21 < A_S \leq 50 \\ 0.1102(A_S - 8.7), & \text{for } A_S > 50 \end{cases}$$

$$\delta = \min(\delta_p, \delta_s)$$

$$\delta_s = 10^{-0.05 A_S'} \quad \text{and} \quad \delta_p = \frac{10^{0.05 A_P'} - 1}{10^{0.05 A_P'} + 1}$$

STEP THIRD:

determine $h_d(n)$;

it is depend on type of filter

WHERE:

Low-Pass FIR Filter

$$h_d(n) = \begin{cases} \left(\frac{2f_c}{F}\right) \frac{\sin 2\pi n f_c / F}{2\pi n f_c / F}, & \text{for } n > 0 \\ \frac{2f_c}{F}, & \text{for } n = 0 \end{cases}$$

where

$$f_c = 0.5 (f_p + f_s) \quad \text{and} \quad \Delta F = f_s - f_p$$

High-Pass FIR Filter

$$h_d(n) = \begin{cases} -\left(\frac{2f_c}{F}\right) \frac{\sin 2\pi n f_c / F}{2\pi n f_c / F}, & \text{for } n > 0 \\ 1 - \frac{2f_c}{F}, & \text{for } n = 0 \end{cases}$$

where

$$f_c = 0.5 (f_p + f_s) \quad \text{and} \quad \Delta F = f_p - f_s$$

Bandpass FIR Filter

$$h_d(n) = \begin{cases} \frac{1}{n\pi} [\sin(2\pi n f_{c2} / F) - \sin(2\pi n f_{c1} / F)], & \text{for } n > 0 \\ \frac{2}{F} (f_{c2} - f_{c1}), & \text{for } n = 0 \end{cases}$$

where

$$f_{c1} = f_{p1} - \frac{\Delta F}{2} \qquad f_{c2} = f_{p2} + \frac{\Delta F}{2}$$

$$\Delta F_l = f_{p1} - f_{s1} \qquad \Delta F_h = f_{s2} - f_{p2}$$

$$\Delta F = \min [\Delta F_l, \Delta F_h]$$

Bandstop FIR Filter

$$h_d(n) = \begin{cases} \frac{1}{n\pi} [\sin(2\pi n f_{c1}/F) - \sin(2\pi n f_{c2}/F)], & \text{for } n > 0 \\ \frac{2}{F}(f_{c1} - f_{c2}) + 1, & \text{for } n = 0 \end{cases}$$

where

$$\begin{aligned} f_{c1} &= f_{p1} + \frac{\Delta F}{2} & f_{c2} &= f_{p2} - \frac{\Delta F}{2} \\ \Delta F_l &= f_{s1} - f_{p1} & \Delta F_h &= f_{p2} - f_{s2} \\ \Delta F &= \min[\Delta F_l, \Delta F_h] \end{aligned}$$

Example 7.10. Design a low-pass digital FIR filter using Kaiser window satisfying the specifications given below.

Passband cut-off frequency, $f_p = 150$ Hz, stopband cut-off frequency, $f_s = 250$ Hz, passband ripple, $A_p = 0.1$ dB, stopband attenuation, $A_s = 40$ dB and sampling frequency, $F = 1000$ Hz.

The length of the filter, $M = 27$

along with the Kaiser window coefficients are listed below.

$h_d(0) = 0.400000006$	$a(0) = 1.000000000$	$h(0) = 0.400000006$
$h_d(1) = 0.302658588$	$a(1) = 0.990451336$	$h(1) = 0.299768597$
$h_d(2) = 0.093381047$	$a(2) = 0.962219954$	$h(2) = 0.089853108$
$h_d(3) = -0.062470987$	$a(3) = 0.916526139$	$h(3) = -0.057256293$
$h_d(4) = -0.075602338$	$a(4) = 0.855326056$	$h(4) = -0.064664647$
$h_d(5) = 0.000160935$	$a(5) = 0.781202257$	$h(5) = 0.000125723$
$h_d(6) = 0.050484315$	$a(6) = 0.697217405$	$h(6) = 0.035198543$
$h_d(7) = 0.026587145$	$a(7) = 0.606746852$	$h(7) = 0.016131667$
$h_d(8) = -0.023507830$	$a(8) = 0.513293743$	$h(8) = -0.012066422$
$h_d(9) = -0.033573132$	$a(9) = 0.420304537$	$h(9) = -0.014110940$
$h_d(10) = 0.000160934$	$a(10) = 0.330991328$	$h(10) = 0.000053268$
$h_d(11) = 0.027559206$	$a(11) = 0.248175934$	$h(11) = 0.006839531$
$h_d(12) = 0.015454730$	$a(12) = 0.174161583$	$h(12) = 0.002691620$
$h_d(13) = -0.014516240$	$a(13) = 0.110641472$	$h(13) = -0.00160609$

Example 7.11 Design a high-pass digital FIR filter using Kaiser window satisfying the specifications given below.

Passband cut-off frequency, $f_p = 3200$ Hz, stopband cut-off frequency, $f_s = 1600$ Hz, passband ripple, $A_p = 0.1$ dB, stopband attenuation, $A_s = 40$ dB and sampling frequency, $F = 10000$ Hz.

Solution From Eq. (7.10), the value of $\delta = 0.005756$.

The actual stopband attenuation, $A_s = 44.796982$ dB.

The value of $\alpha = 3.952357$ and $D = 2.565946$ from Eq. (7.11).

The length of the filter, $M = 18$

The desired filter coefficients $\{h_d(n)\}$ are obtained from Eq. (7.12). The filter coefficients of the non-causal digital filter $\{h(n) = h(-n)\}$ along with the Kaiser window coefficients are listed below.

The filter coefficients of the non-causal digital filter $\{h(n) = h(-n)\}$ along with the Kaiser window coefficients are listed below.

$a(0) = 0.519999981$	$a(0) = 1.000000000$	$h(0) = 0.519999981$
$a(1) = -0.317566037$	$a(1) = 0.976742625$	$h(1) = -0.310180277$
$a(2) = -0.019747764$	$a(2) = 0.909421921$	$h(2) = -0.017959049$
$a(3) = 0.104217999$	$a(3) = 0.805053890$	$h(3) = 0.083901107$
$a(4) = 0.019595038$	$a(4) = 0.674255788$	$h(4) = 0.013212068$
$a(5) = -0.060581177$	$a(5) = 0.529811919$	$h(5) = -0.032096628$
$a(6) = -0.019342067$	$a(6) = 0.384986669$	$h(6) = -0.007446438$

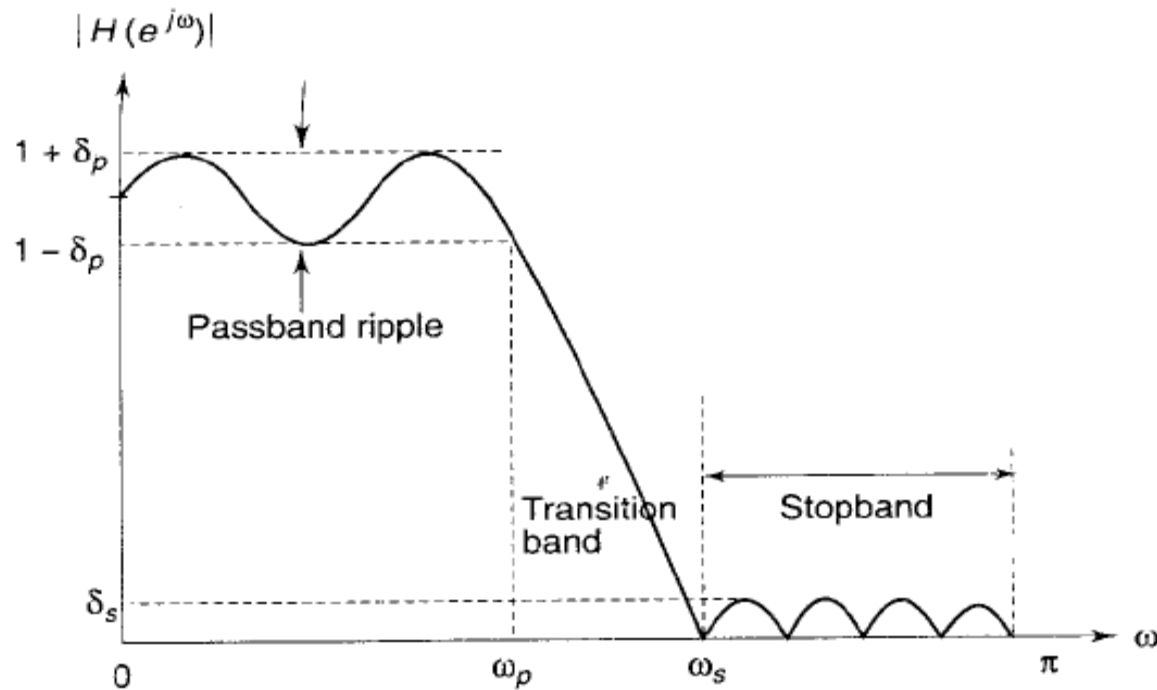
DESIGN OF OPTIMAL LINEAR PHASE FIR FILTERS

$$1 - \delta_p \leq |H(e^{j\omega})| \leq 1 + \delta_p, \quad |\omega| \leq \omega_p$$

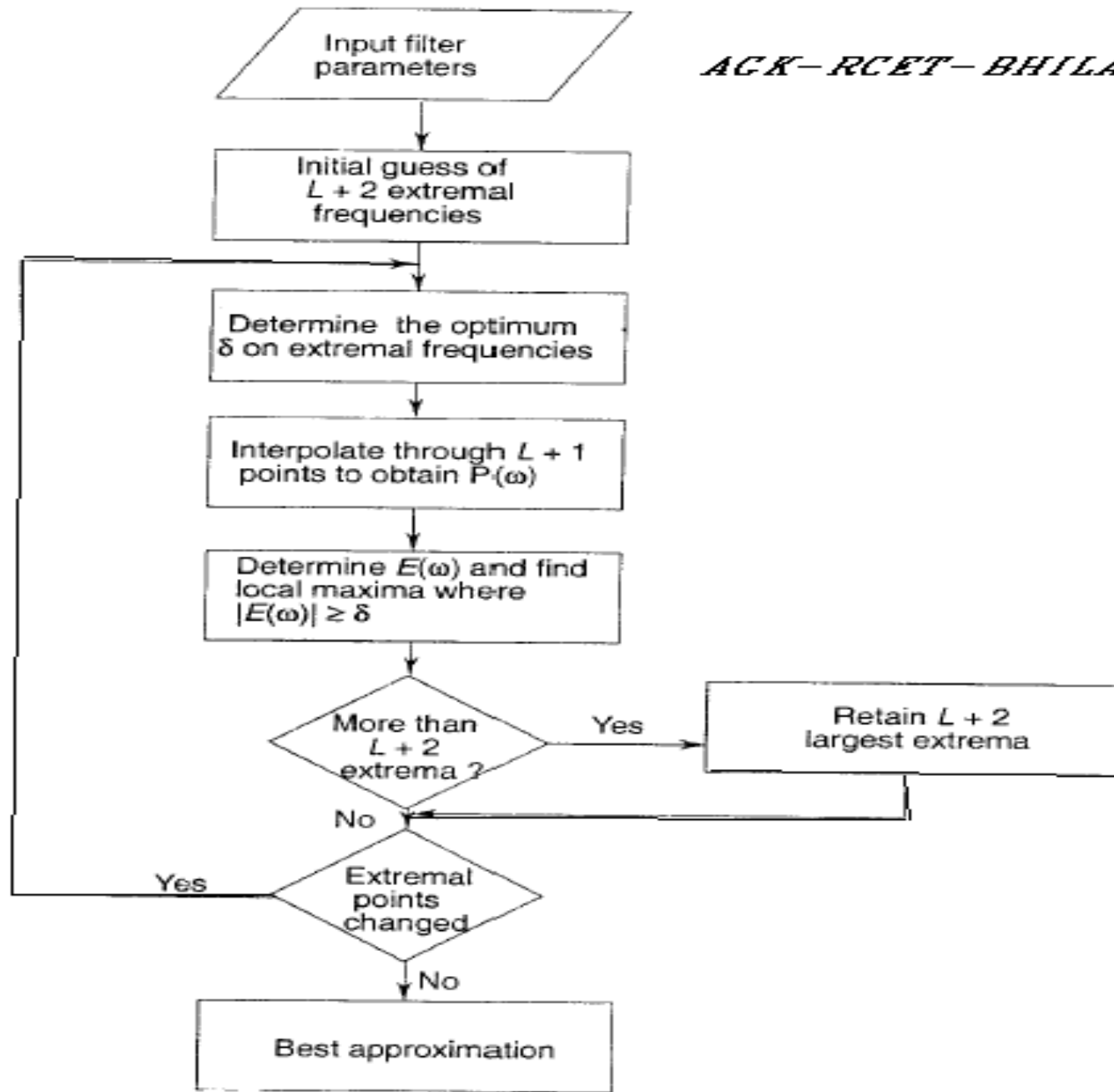
The frequency response in the stopband is

$$- \delta_s \leq |H(e^{j\omega})| \leq \delta_s, \quad |\omega| \geq \omega_s$$

The term δ_p represents the passband ripple and δ_s is the maximum attenuation in the stopband.



Frequency Response Characteristics of Physically Realisable Filters



Flowchart of the Remez Exchange Algorithm

- 7.13 What are the effects of truncating an infinite Fourier series into a finite series ?
- 7.14 Explain Gibb's phenomenon.
- 7.15 What are the desirable features of the window functions ?
- 7.16 What are the effects of windowing ?
- 7.17 Explain the process of windowing using illustrations.
- 7.18. Name the different types of window functions. How they are defined ?
- 7.19 What is a rectangular window function ? Obtain its frequency-domain characteristics.
- 7.20 What is a Hamming window function ? Obtain its frequency-domain characteristics.
- 7.21 What is a Hann window function ? Obtain its frequency-domain characteristics.
- 7.22 Compare the frequency-domain characteristics of the different types of window functions.
- 7.23 The desired frequency response of a low-pass filter is

$$H_d(e^{j\omega}) = \begin{cases} 1, & -\pi/2 \leq \omega \leq \pi/2 \\ 0, & \pi/2 \leq |\omega| < \pi \end{cases}$$

Determine $h_d(n)$. Also determine $h(n)$ using the symmetric rectangular window with window length = 7.

Ans: $h_d(-3) = -0.1061 = h_d(3)$, $h_d(-2) = 0 = h_d(2)$, $h_d(-1) = 0.3183 = h_d(1)$, $h_d(0) = 0.5$; $h(n) = h_d(n)$, $w(n) = h_d(n)$ for $-3 \leq n \leq 3$

- 24 The desired frequency response of a low-pass filter is

24 The desired frequency response of a low-pass filter is

$$H_d(e^{j\omega}) = \begin{cases} e^{-j3\omega}, & -3\pi/4 \leq \omega \leq 3\pi/4 \\ 0, & 3\pi/4 < |\omega| \leq \pi \end{cases}$$

Determine $H(e^{j\omega})$ for $M = 7$ using a rectangular window.

Ans: $H(e^{j\omega}) = e^{-j3\omega} [0.75 + 0.4502 \cos \omega - 0.3184 \cos 2\omega + 0.15 \cos 3\omega]$

25 Design a bandpass filter which approximates the ideal filter with cut-off frequencies at 0.2 rad/sec and 0.3 rad/sec. The filter order is $M = 7$. Use the Hanning window function.

Ans: $h(0) = 0, h(1) = 0.0078, h(2) = 0.0209, h(3) = 0.0232, h(4) = 0.0128, h(5) = 0.00248, h(6) = 0$

26 What is a Kaiser window? In what way is it superior to other window functions?

27 Explain the procedure for designing an FIR filter using the Kaiser window.

- 7.28 *What is an FIR half-band digital filter ? Explain with a suitable illustration.*
- 7.29 *What is an optimal linear phase FIR filter ? What parameters are optimised in these filters ?*
- 7.30 *State and explain the alternation theorem.*
- 7.31 *What are extra ripple filters ?*
- 7.32 *What are maximal ripple filters ?*
- 7.33. *Explain the Remez exchange algorithm used in the design of optimal filters.*

THANK YOU

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