

# HEAT TRANSFER BY CONVECTION

## CONDUCTION

Mechanism of heat transfer through a solid or fluid in the **absence** any fluid motion.

## CONVECTION

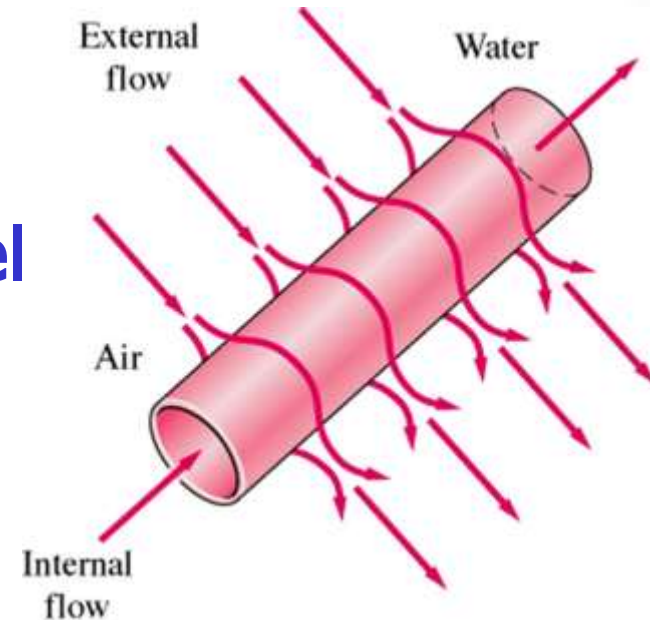
Mechanism of heat transfer through a fluid in the **presence** of bulk fluid motion

- **Natural (free) Convection**
- **Forced Convection**

(depending on how the fluid motion is initiated)

# CLASSIFICATION OF FLUID FLOWS

- **Viscous-inviscid**
- **Internal flow-  
External flow**
- **Open-closed channel**
- **Compressible-  
Incompressible**
- **Laminar-  
Turbulent**
- **Natural- Forced**
- **Steady- Unsteady**
- **One-,two-,three-  
dimensional**



# VISCOSITY

When two fluid layers move relative to each other, a friction force develops between them and the slower layer tries to slow down the faster layer.

## internal resistance to flow

- cohesive forces between the molecules in liquid
- molecular collisions in gases.

**Viscous flows:** viscous effects are significant

**Inviscid flow regions:** viscous forces are negligibly small compared to inertial or pressure forces.

→ measure of stickiness or resistance to deformation

1. Kinematic viscosity
2. Dynamic viscosity

# VISCOSITY DEPENDS ON

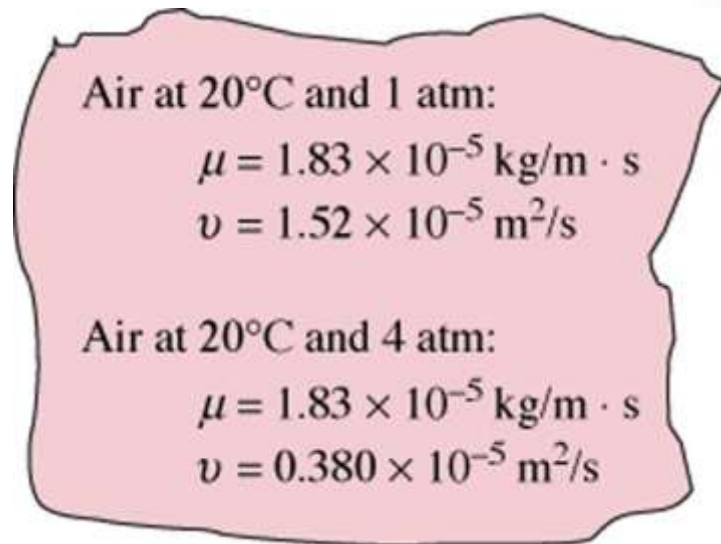
- **TEMPERATURE**
- **PRESSURE**

For liquids dependence of pressure is negligible

For gases kinematic viscosity depends on pressure since its relation to density

$\mu$  Dynamic viscosity  
(kg/m.s or poise)

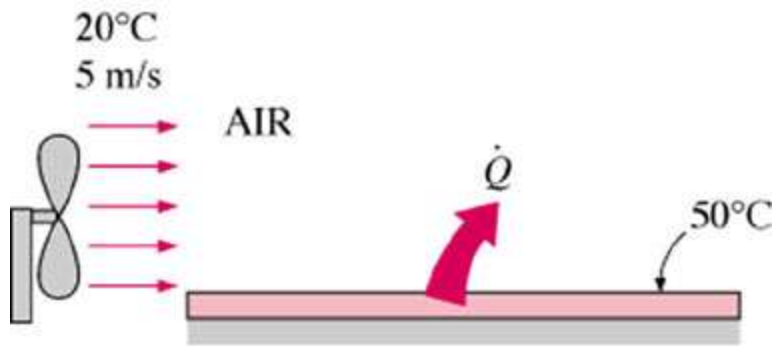
$$\nu = \frac{\mu}{\rho}$$



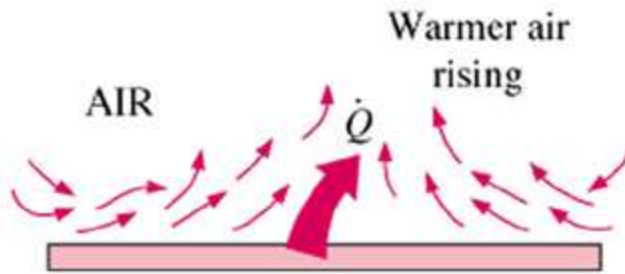
Air at 20°C and 1 atm:  
 $\mu = 1.83 \times 10^{-5} \text{ kg/m} \cdot \text{s}$   
 $\nu = 1.52 \times 10^{-5} \text{ m}^2/\text{s}$

Air at 20°C and 4 atm:  
 $\mu = 1.83 \times 10^{-5} \text{ kg/m} \cdot \text{s}$   
 $\nu = 0.380 \times 10^{-5} \text{ m}^2/\text{s}$

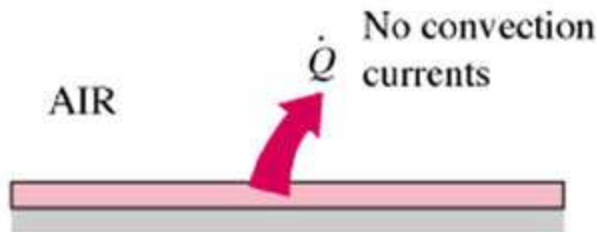
$\nu$  Kinematic viscosity,  
 $\text{m}^2/\text{s}$  or stroke



(a) Forced convection



(b) Free convection



(c) Conduction

## Convection heat transfer

- Dynamic viscosity
- Thermal conductivity
- Density
- Specific heat
- Fluid velocity
- Geometry
- Roughness
- Type of fluid flow

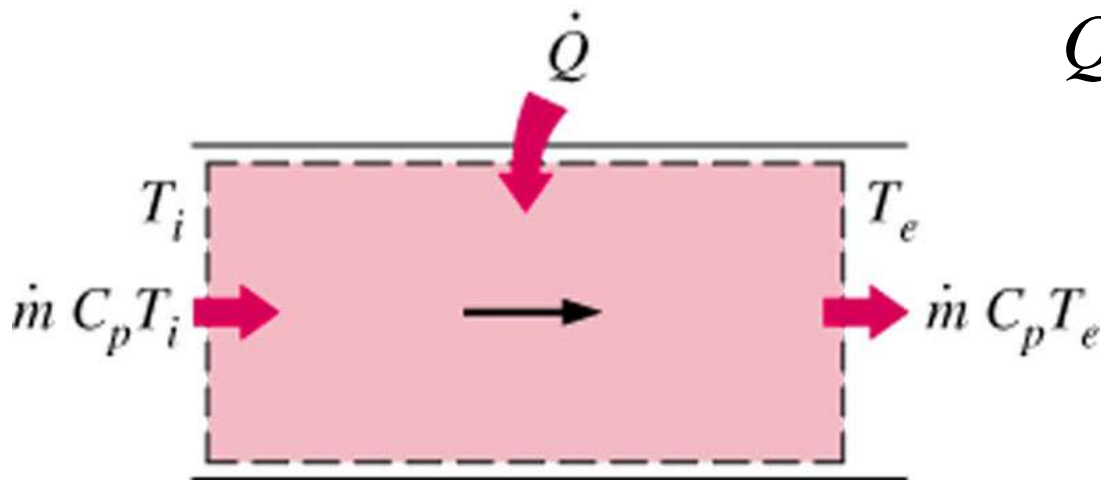
# NEWTON'S LAW OF COOLING

$$\dot{Q}_{conv} = hA_S (T_S - T_\infty) \quad (\text{W})$$

$h$  Convection heat transfer coefficient ( $\text{W}/\text{m}^2 \cdot ^\circ\text{C}$ )

The rate of heat transfer between a solid surface and a fluid per unit surface area per unit temperature difference

# GENERAL THERMAL ANALYSIS



Energy balance:

$$\dot{Q} = \dot{m} C_p (T_e - T_i)$$

$$\dot{Q}_{conv} = hA_S (T_S - T_\infty)$$

$$\dot{Q} = \dot{m} C_p (T_e - T_i)$$



# FORCED CONVECTION

- **LAMINAR FLOW**

Smooth streamlines

Highly- ordered motion

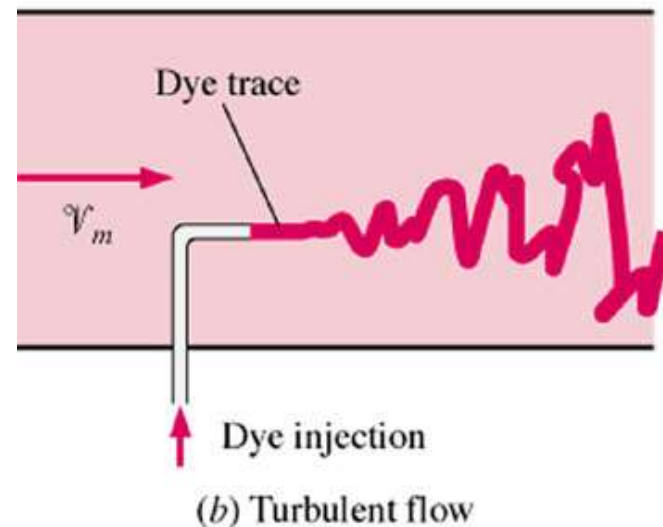
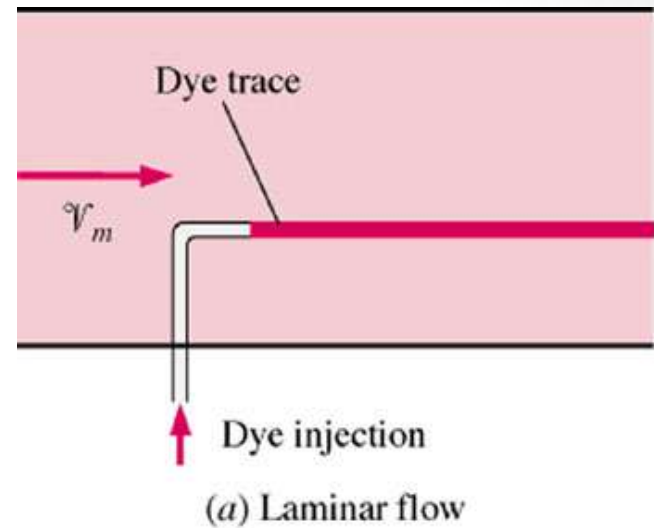
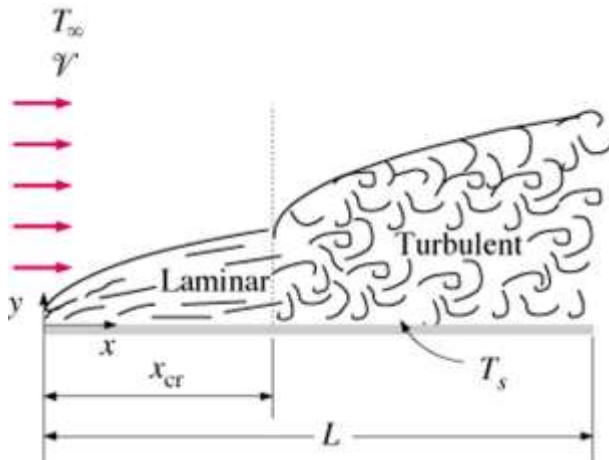
(highly viscous fluids in small pipes)

- **TURBULENT FLOW**

Velocity fluctuations

Highly-disordered motion

- **TRANSITIONAL FLOW**



# REYNOLDS NUMBER

Flow Regime:

Geometry

Surface roughness

Flow velocity

Surface temperature  
type of fluid

Ratio of the inertial forces to  
viscous forces in the fluid

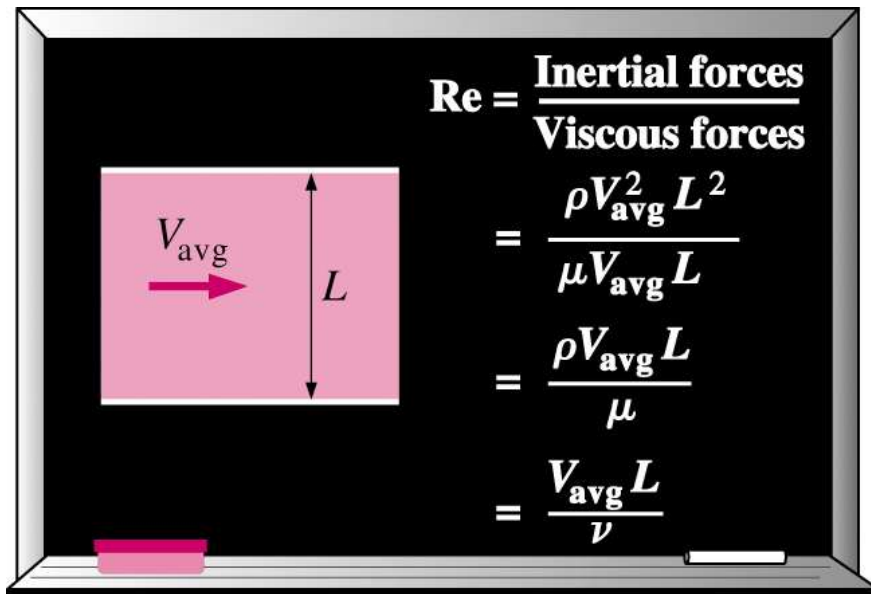
$$\text{Re} = \frac{v_m D}{\nu} = \frac{\rho v_m D}{\mu}$$

$v_m$  Mean flow velocity

$D$  Characteristic length of  
the geometry

$\nu = \mu / \rho$  Kinematic viscosity

## Definition of Reynolds number



- Critical Reynolds number ( $Re_{cr}$ ) for flow in a round pipe

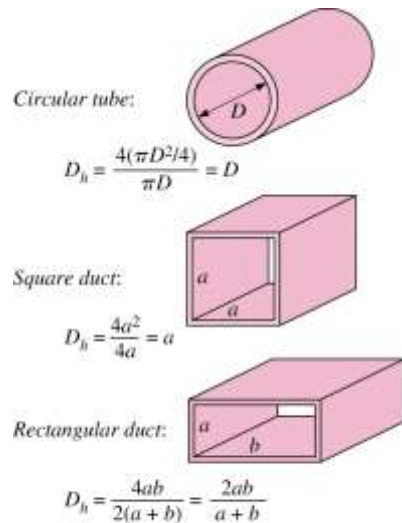
$Re < 2300 \Rightarrow$  laminar

$2300 \leq Re \leq 4000 \Rightarrow$  transitional

$Re > 4000 \Rightarrow$  turbulent

- Note that these values are approximate.
- For a given application,  $Re_{cr}$  depends upon
  - Pipe roughness
  - Vibrations
  - Upstream fluctuations, disturbances (valves, elbows, etc. that may disturb the flow)

# HYDRAULIC DIAMETER



- For non-round pipes,
- the hydraulic diameter

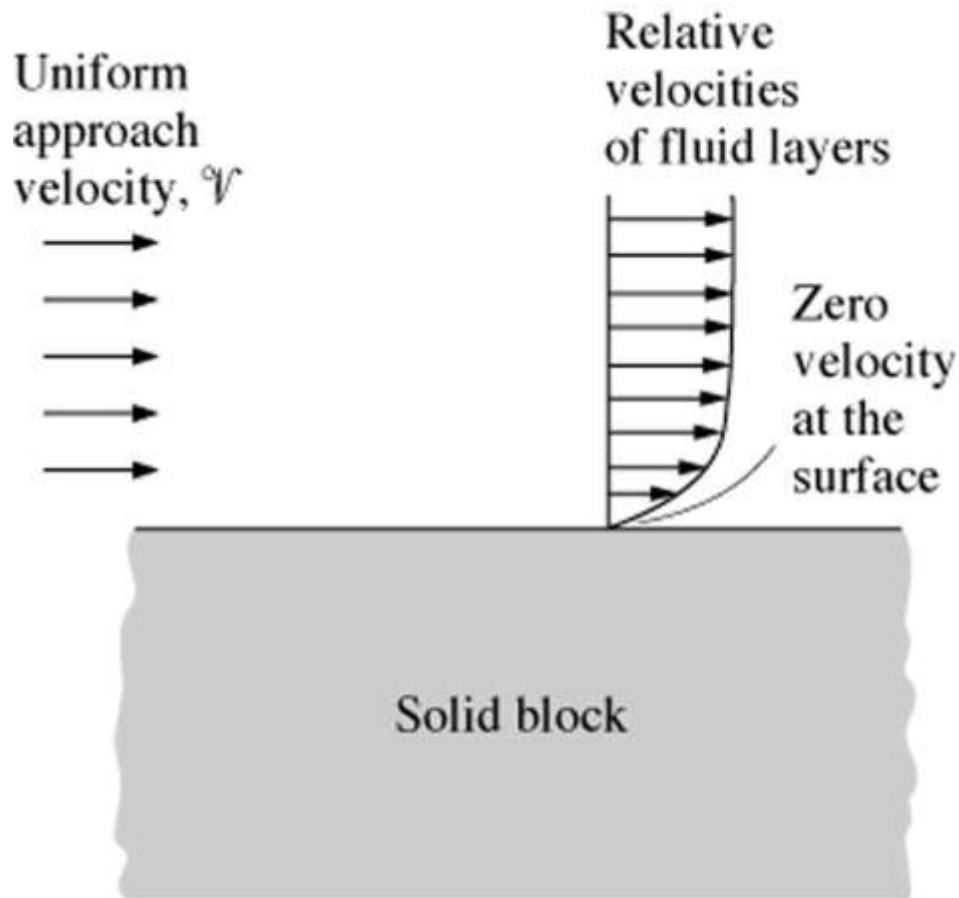
$$D_h = 4A_c/P$$

$A_c$  = cross-section area

$P$  = wetted perimeter

# Velocity

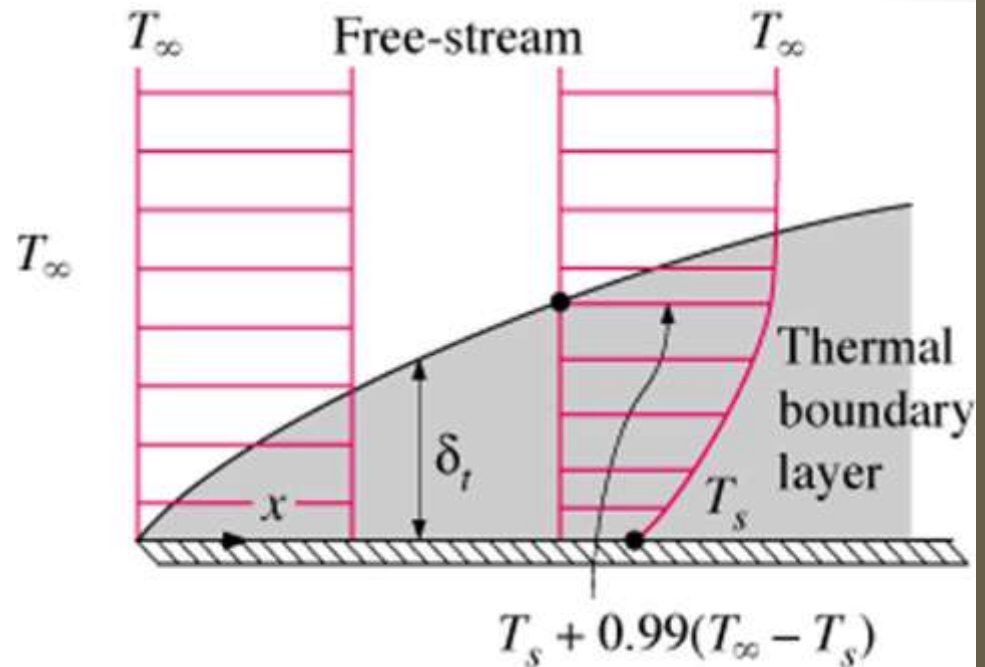
## No-slip condition



# THERMAL BOUNDARY LAYER

Flow region over the surface in which the temperature variation in the direction normal to the surface

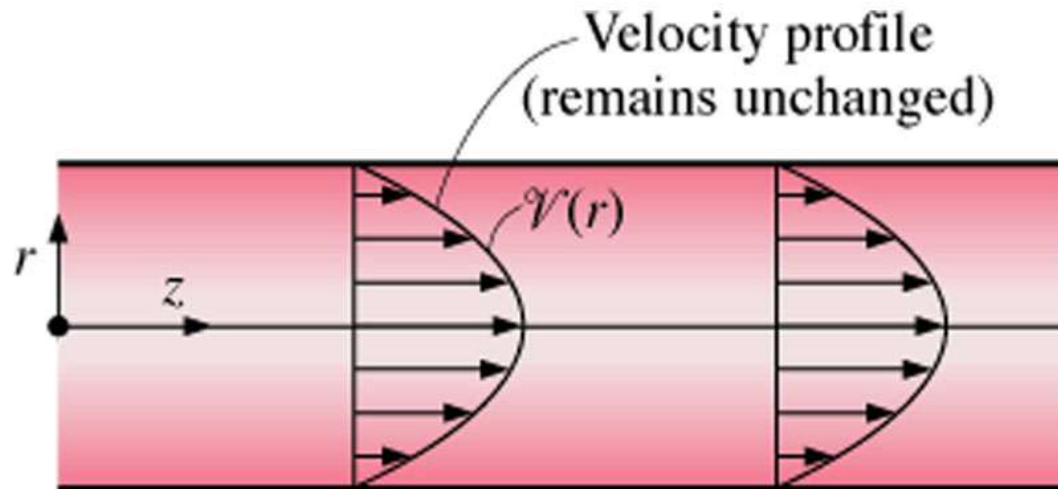
Velocity profile influences temperature profile



# VELOCITY

A flow field is best characterized by the velocity distribution, and velocity may vary in three dimension

$\vec{V}(x, y, z)$  in rectangular       $\vec{V}(r, \theta, z)$  in cylindrical coordinates



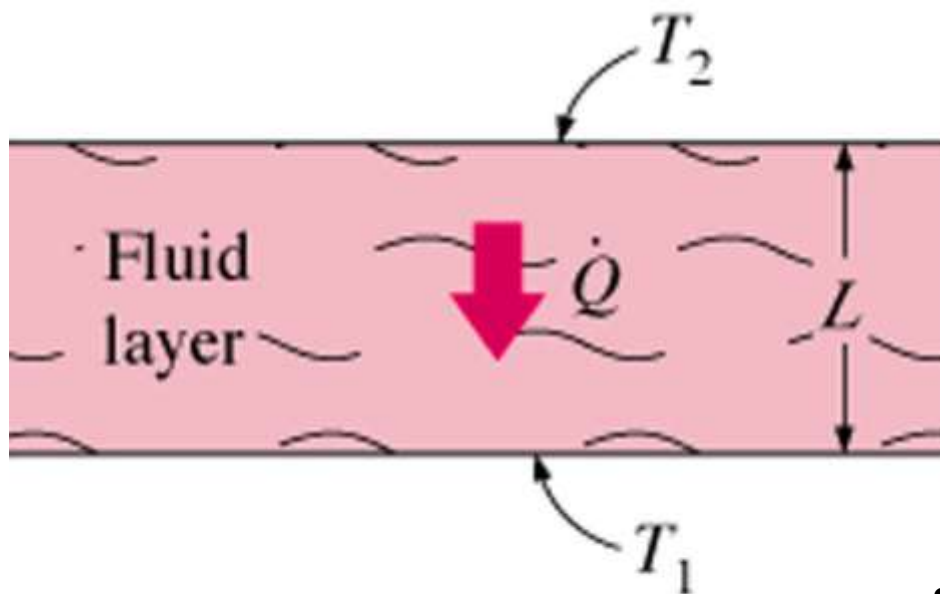
One dimensional flow in a circular pipe

In which direction does the velocity change in this figure???



# NUSSELT NUMBER

(Dimensionless number)



$$\Delta T = T_2 - T_1$$

$$Nu = \frac{hL_c}{k}$$

- $q_{cond} = k \frac{\Delta T}{L}$

- $q_{conv} = h\Delta T$

- $\frac{q_{conv}}{q_{cond}} = \frac{h\Delta T}{k\Delta T / L} = \frac{hL}{k} = Nu$

# PRANDTL NUMBER

- Boundary layer theory

$$\text{Pr} = \frac{\mu C_p}{k}$$

$$\text{Pr} = \frac{\text{molecular diffusivity of momentum}}{\text{molecular diffusivity of heat}} = \frac{\nu}{\alpha} = \frac{\mu C_p}{k}$$

$\text{Pr} \ll 1$  heat diffuses very quickly in liquid metals,  $t_b/l$  thicker

$\text{Pr} \gg 1$  heat diffuses very slowly in oils relative to momentum,  $t_b/l$  thinner than  $\nu b/l$

# PARALLEL FLOW OVER FLAT PLATES

$$\text{Re}_{cr} = \frac{\rho U x_{cr}}{\mu} = 5 \times 10^5$$

$$Nu = \frac{hL}{k} = 0.664 \text{ Re}_L^{0.5} \text{ Pr}^{1/3}$$

$$\text{Re}_L < 5 \times 10^5 \quad \text{laminar}$$

$$Nu = \frac{hL}{k} = 0.037 \text{ Re}_L^{0.8} \text{ Pr}^{1/3}$$

$$0.6 \leq \text{Pr} \leq 60 \quad \text{turbulent}$$

$$5 \times 10^5 \leq \text{Re}_L \leq 10^7$$

# NATURAL CONVECTION

# CONVECTIVE HEAT TRANSFER COEFFICIENT

Coefficient of volume expansion

Grashof number

$$Gr_L = \frac{g\beta(T_s - T_\infty)L_C^3}{\nu^2}$$

viscosity

Rayleigh number

$$Ra_L = Gr_L Pr$$

Prandtl number

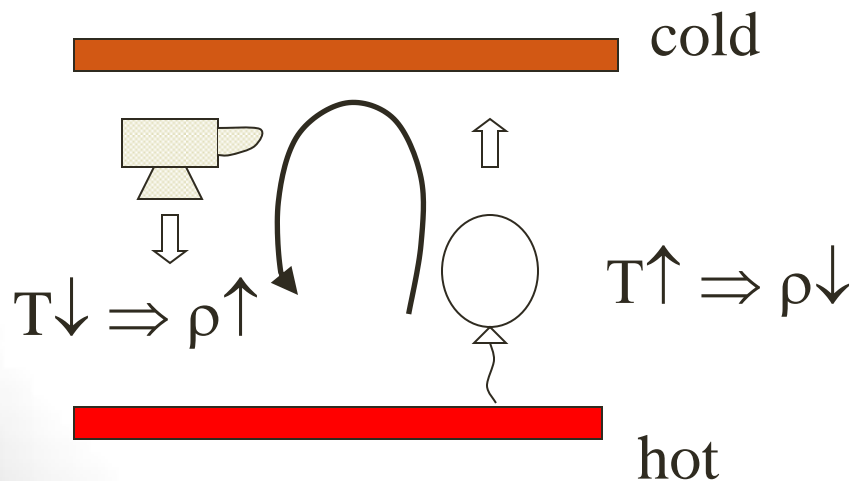
Nusselt number

$$Nu = \frac{hL_C}{k} = CRa_L^n$$

Table 20-1

# Free Convection

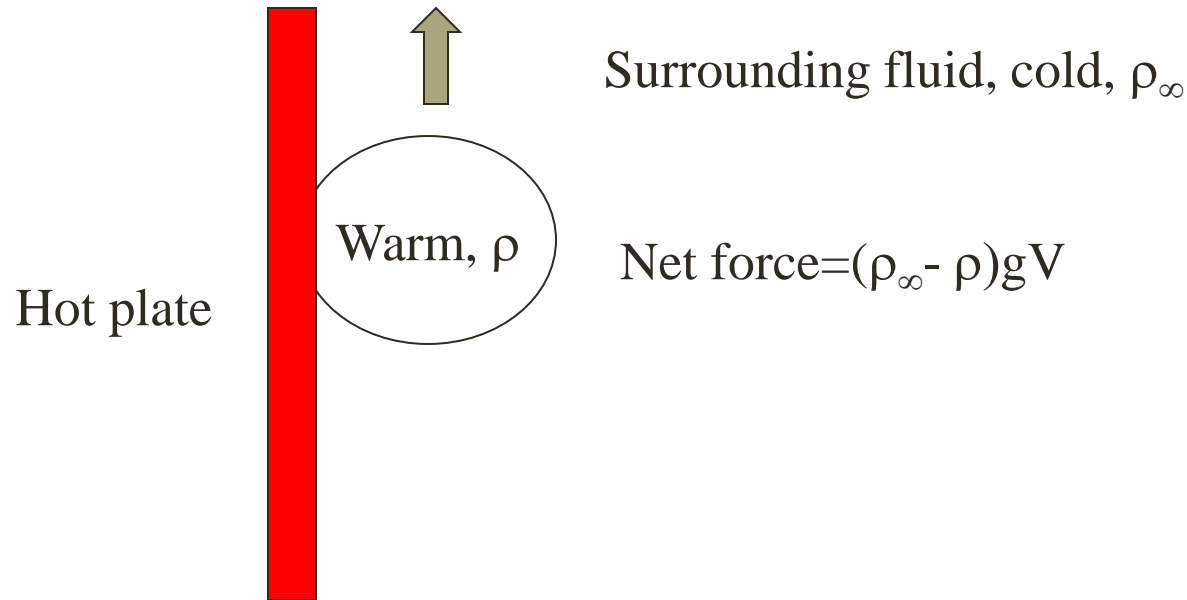
A free convection flow field is a self-sustained flow driven by the presence of a temperature gradient. (As opposed to a forced convection flow where external means are used to provide the flow.) As a result of the temperature difference, the density field is not uniform also. Buoyancy will induce a flow current due to the gravitational field and the variation in the density field. In general, a free convection heat transfer is usually much smaller compared to a forced convection heat transfer. It is therefore important only when there is no external flow exists.



Flow is unstable and a circulatory pattern will be induced.

# Basic Definitions

Buoyancy effect:



The density difference is due to the temperature difference and it can be characterized by their volumetric thermal expansion coefficient,  $\beta$ :

$$\beta = -\frac{1}{\rho} \left( \frac{\partial \rho}{\partial T} \right)_P \approx -\frac{1}{\rho} \frac{\rho_\infty - \rho}{T_\infty - T} = -\frac{1}{\rho} \frac{\Delta \rho}{\Delta T}$$

$$\Delta \rho \approx \beta \Delta T$$

# Grashof Number and Rayleigh Number

Define Grashof number,  $Gr$ , as the ratio between the buoyancy force and the viscous force:

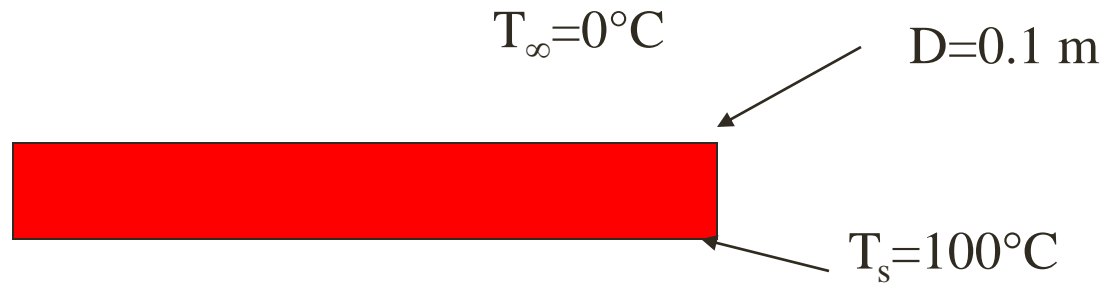
$$Gr = \frac{g \beta \Delta T L^3}{\nu^2} = \frac{g \beta (T_s - T_\infty) L^3}{\nu^2}$$

- Grashof number replaces the Reynolds number in the convection correlation equation. In free convection, buoyancy driven flow sometimes dominates the flow inertia, therefore, the Nusselt number is a function of the Grashof number and the Prandtl number alone.  $Nu=f(Gr, Pr)$ . Reynolds number will be important if there is an external flow. (see chapter 11.5, combined forced and free convection).
- In many instances, it is better to combine the Grashof number and the Prandtl number to define a new parameter, the Rayleigh number,  $Ra=GrPr$ . The most important use of the Rayleigh number is to characterize the laminar to turbulence transition of a free convection boundary layer flow. For example, when  $Ra>10^9$ , the vertical free convection boundary layer flow over a flat plate becomes turbulent.



# Example

Determine the rate of heat loss from a heated pipe as a result of natural (free) convection.



Film temperature ( $T_f$ ): averaged boundary layer temperature  $T_f = 1/2(T_s + T_{\infty}) = 50^{\circ}\text{C}$ .  
 $k_f = 0.03 \text{ W/m.K}$ ,  $\text{Pr} = 0.7$ ,  $\nu = 2 \times 10^{-5} \text{ m}^2/\text{s}$ ,  $\beta = 1/T_f = 1/(273 + 50) = 0.0031 \text{ (1/K)}$

$$Ra = \frac{g\beta(T_s - T_{\infty})L^3}{\nu^2} \text{Pr} = \frac{(9.8)(0.0031)(100 - 0)(0.1)^3}{(2 \times 10^{-5})^2} (0.7) = 7.6 \times 10^6.$$

$$Nu_D = \left\{ 0.6 + \frac{0.387 Ra^{1/6}}{[1 + (0.559 / \text{Pr})^{9/16}]^{8/27}} \right\}^2 = 26.0 \quad (\text{equation 11.15 in Table 11.1})$$

$$h = \frac{k_f}{D} Nu_D = \frac{0.03}{0.1} (26) = 7.8 \text{ (W / m}^2 \text{ K)}$$

$$q = hA(T_s - T_{\infty}) = (7.8)(\pi)(0.1)(1)(100 - 0) = 244.9 \text{ (W)}$$

Can be significant if the pipe are long.