

Unit - 1 (Mrs. Samta Deshpande)

WATER

Specification for Water –

Surface and ground water normally used for domestic purposes. Each industry has its own specification for water.

1) Textile industry-

Specification –

- Water should be soft, free from turbidity.
- Free from colour, Fe and Mn ion.

Remarks –

- Hard water creates uneven dyeing which causes stains of fabrics.
- Hard water decreases the solubility of dyes.

2) Laundries-

Specification-

- Water should be soft, free from colour.
- Free from organic matter. Free from Fe and Mn.

Remarks –

- Hard water increases consumption of soaps.
- Salts of Fe and Mn creates gray or yellow colour on fabric.

3) Beverages-

Specification-

- Water should not be alkaline.

Remarks-

- Alkalinity destroys the taste.
- Neutralization occurs.

4) Dairies and industries-

Specification-

- Water should be colorless, tasteless, odorless.
- Free from pathogenic organism.

Remarks-

- Organic matter imparts foul smell.

5) Boilers-

Specification-

- Water should be zero hardness.

Remarks-

- Scale formation on using hard water.
- Loss of heat.

6) Paper Industry -

Specification-

- Water should be free from SiO₂, turbidity,
- Free from alkalinity.
- Free from hardness.

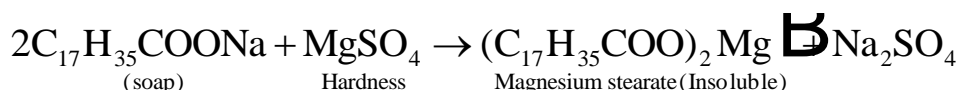
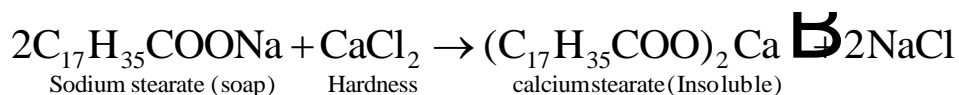
Remarks-

- SiO₂ produces cracks on paper.
- Brightness and colour of the paper affected.

HARDNESS OF WATER

Those water which does not produce lather with soap are termed as hard water. On the other hand soft water readily produce a lot of lather when mixed with a little of soap. The hard water causes boiler troubles like scale formation etc. the hardness is mostly due to the presence of bivalent metallic ions which react with soap and form precipitates. Some major bivalent cations are Mg⁺⁺, Ca⁺⁺ and Fe⁺⁺. Some important anions are HCO₃⁻, NO₃⁻, SO₄⁻ etc.

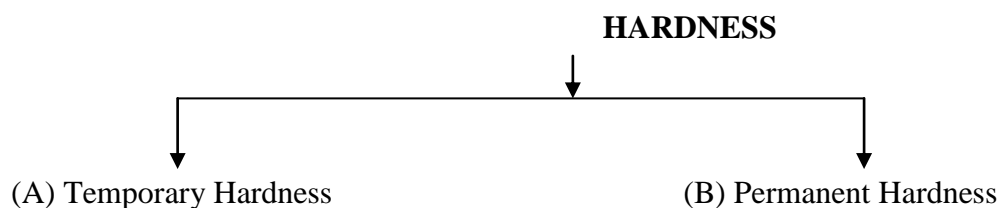
Example :- A reaction of soap (Sodium stearate) with calcium chloride and Magnesium sulphate is as follows-



The water are commercially classified on the basis of degree of hardness as follows-

Hardness	Name of the water
0-70 mg/litre	Soft water
70-150 mg/litre	Moderate hard water
150-300 mg/litre	Hard water
300 mg/litre and above	Very hard water

Types of Hardness



or

or

Carbonate Or Alkaline Hardness

Non Carbonate or Non alkaline Hardness

(A) Temporary Hardness -	(B) Permanent Hardness-
<p>(i) It is caused by the presence of dissolved bicarbonates of calcium, magnesium and other heavy metals.</p> <p>(ii) Salts which are responsible for temporary hardness are – $\text{Ca}(\text{HCO}_3)_2$ and $\text{Mg}(\text{HCO}_3)_2$</p> <p>(iii) It can be removing by simple boiling of water.</p> <p>(iv) Bicarbonates are decomposed and are converted into insoluble carbonates or hydroxides, which precipitate and settle down at the bottom of the vessel.</p> $\text{Mg}(\text{HCO}_3)_2 \xrightarrow{\text{Heat}} \text{Mg}(\text{OH})_2 + 2\text{CO}_2 + \text{CO}_2 \uparrow$ <p>(v) It is also known as carbonate or Alkaline hardness.</p>	<p>(i) It is caused by the presence of soluble chlorides and sulphates of calcium, Magnesium, iron and other heavy metals.</p> <p>(ii) Salts which are responsible for permanent hardness are – CaCl_2, MgCl_2, CaSO_4, FeSO_4, $\text{Al}_2(\text{SO}_4)_3$.</p> <p>(iii) It can't be removed by simply boiling of water.</p> <p>(iv) It is also known as non carbonate or non alkaline hardness.</p>

DEGREE OF HARDNESS

Hardness of water is expressed as **equivalent of calcium carbonate (CaCO_3)**.

The reason for choosing CaCO_3 as standard is – CaCO_3 is the ease in calculations as its molecular weight is exactly 100.

It is most insoluble salt that can be precipitated in water treatment.

Equivalent of CaCO_3 =

$$= \frac{\text{Mass of hardness – producing substance} \times 50}{\text{Chemical equivalent of hardness – producing substance}}$$

Multiplication factors for different salt are tabulated

(i) Table -

Dissolved salt	Molar mass	Chemical equivalent	Multiplication factor for converting into equivalents of CaCO_3 .
$\text{Ca}(\text{HCO}_3)_2$	162	81	100/162
$\text{Mg}(\text{HCO}_3)_2$	146	73	100/146
CaSO_4	136	68	100/136
MgSO_4	120	60	100/120
CaCl_2	111	55.5	100/111

MgCl ₂	95	47.5	100/95
CaCO ₃	100	50	100/100
MgCO ₃	84	42	100/84
CO ₂	44	22	100/44
Mg(NO ₃) ₂	148	74	100/148
HCO ₃ ⁻	61	61	100/122
OH ⁻	17	17	100/34
CO ₃ ²⁻	60	30	100/60
NaAlO ₂	82	82	100/164
Al ₂ (SO ₄) ₃	342	57	100/114
FeSO ₄ .7H ₂ O	278	139	100/278
H ⁺	1	1	100/2

UNIT OF HARDNESS-

UNIT
↓

- (A) Parts per million (ppm)
- (B) Milligrams per litre (Mg/L)
- (C) Degree Clark (°Cl)
- (D) Degree French (°Fr)

(A) Parts per Million (ppm) – It is defined as the number of parts of CaCO₃ equivalent hardness per 10⁶ parts of water.

∴ 1ppm = 1 part of CaCO₃ equivalent hardness in 10⁶ parts of water.

(B) Milligrams per litre (Mg/L) – It is defined as the number of milligrams of CaCO₃ present in one litre of water.

∴ 1 Mg/L = 1 mg of CaCO₃ equivalent hardness per litre of water.

1Mg/L = 1 ppm

(C) Degree Clark (°Cl) - It is defined as the parts of CaCO₃ equivalent hardness per 70,000 parts of water.

Or

It is the number of grains of CaCO₃ equivalent hardness for a gallon of water.

∴ 1 °Cl = 1 part of CaCO₃ per 70,000 parts of water.

(D) Degree French ($^{\circ}\text{Fr}$) – It is defined as the parts of CaCO_3 equivalent hardness per 10^5 parts of water.

$\therefore 1^{\circ}\text{Fr} = 1$ part of CaCO_3 equivalent hardness per 10^5 parts of water.

Relationship between various units.

$$\begin{aligned} 1 \text{ ppm} = 1 \text{ Mg/L} &= 0.1^{\circ}\text{Fr} &= 0.07^{\circ}\text{Cl} \\ 1 \text{ mg/l} = 1 \text{ ppm} &= 0.1^{\circ}\text{Fr} &= 0.07^{\circ}\text{Cl} \\ 1^{\circ}\text{Cl} = 1.43^{\circ}\text{Fr} &= 14.3 \text{ ppm} &= 14.3 \text{ mg/L} \\ 1^{\circ}\text{Fr} = 10 \text{ ppm} &= 10 \text{ Mg/L} &= 0.7^{\circ}\text{Cl} \end{aligned}$$

Hence ;

$$1 \text{ ppm} = 0.1^{\circ}\text{Fr} = 0.07^{\circ}\text{Cl} = 1 \text{ mg/L}$$

Solved examples based on determination of Hardness of water

Ex.(1) A water sample contains 500 mg of CaSO_4 per litre. Calculate the hardness in terms of CaCO_3 equivalents.

Solution:-

Hardness = (Mass of CaSO_4 in Mg/L) X Multiplication factor

$$= \text{Mass of } \text{CaSO}_4 \text{ in Mg / L} \times \left\{ \frac{\text{chemical eq. of } \text{CaCO}_3}{\text{chemical eq. of } \text{CaSO}_4} \right\}$$

$$= 500 \text{ mg / L} \times \frac{50}{80}$$

$$= 312.5 \text{ Mg/L} = 312.5 \text{ ppm. Ans}$$

Ex. (2) How many grams of MgCO_3 dissolved per litre gives 90 ppm of hardness.

Solution-

$$\text{Hardness} = (\text{Mass of } \text{MgCO}_3 \text{ in mg / L}) \times \left\{ \frac{\text{chemical eq. of } \text{CaCO}_3}{\text{chemical eq. of } \text{MgCO}_3} \right\}$$

$$\text{Mass of } \text{MgCO}_3 = \text{Hardness} \times \frac{\text{chemical eq. of } \text{MgCO}_3}{\text{chemical eq. of } \text{CaCO}_3}$$

$$\text{Mass of } \text{MgCO}_3 = 90 \text{ ppm} \times \frac{42}{50}$$

$$= 75.6 \text{ Mg/L} = 75.6 \text{ ppm Ans.}$$

Thus 75.6×10^{-3} gm of MgCO_3 dissolved per litre gives 90 ppm of hardness.

Ex. (3) A sample of 70,000 c.c. of hard water bearing dissolved impurities gave on analysis the following results-

$$\begin{aligned} \text{MgCl}_2 &= 9.50 \text{ gm} \\ \text{CaSO}_4 &= 13.60 \text{ gm} \\ \text{Ca(HCO}_3)_2 &= 16.20 \text{ gm} \end{aligned}$$

Calculate the degree of hardness in Clark's, French and in ppm scales.

Solution:-

$$\begin{array}{ccccccc} \text{MgCl}_2 & = & \text{CaSO}_4 & = & \text{Ca(HCO}_3)_2 & = & \text{CaCO}_3 \\ 24+71 & & 40+32+64 & & 40+2(1+12+48) & & 40+12+48 \\ = 95 & & = 126 & & = 162 & & = 100 \end{array}$$

$$95 \text{ gm of MgCl}_2 = 100 \text{ gm CaCO}_3$$

$$\begin{aligned} 9.50 \text{ gm of MgCl}_2 &= \frac{100}{95} \times 9.5 \\ &= 10 \text{ gm of CaCO}_3. \end{aligned}$$

$$\therefore 136 \text{ gm of CaSO}_4 = 100 \text{ gm of CaCO}_3$$

$$13.6 \text{ gm of CaSO}_4 \times \frac{100}{136} = 10 \text{ gm CaCO}_3$$

$$162 \text{ gm of Ca(HCO}_3)_2 = 100 \text{ gm of CaCO}_3$$

$$\therefore 16.2 \text{ gm of Ca(HCO}_3)_2 \times \frac{100}{162} = 10 \text{ gm CaCO}_3$$

Total weight of hardness causing substance in terms of CaCO₃ = 10 + 10 + 10 = 30 gm

Thus total hardness of water in terms of CaCO₃ is 30 gm per 70,000 C.C. (70,000 gm) of water.

(i) Clark's degree of hardness = 30°Cl (Clark's)

(ii) 7° Clark's scale = 10° French scale

$$\begin{aligned} 30^\circ \text{ Clark's scale} &= (10/7) \times 30 \\ &= 42.857^\circ \text{ French} \end{aligned}$$

10° French scale = 100 ppm

42.857° French scale (100/10) X 42.857 = 428.57 ppm

Ex. (4) Calculate temporary hardness and total hardness of sample of water containing Mg(HCO₃)₂ = 7.3

Mg/L, Ca(HCO₃)₂ = 16.2 Mg/L, MgCl₂ = 9.5 Mg/L, CaSO₄ = 13.6 Mg/L

Solution:-

$$\begin{aligned} \text{Temporary Hardness} &= \frac{9.5}{95} \times \frac{100}{146} + 16.2 \times \frac{100}{162} \text{ Mg/L} \\ &= (5 + 10) \text{ Mg/L} \end{aligned}$$

$$= 15 \text{ Mg/L}$$

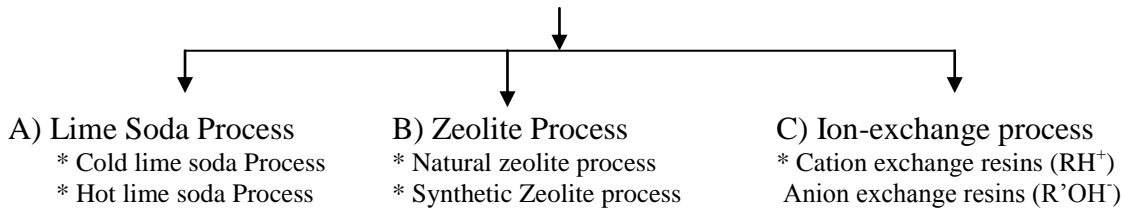
$$\text{Permanent hardness} = 10 \times \frac{100}{95} + 13.6 \times \frac{100}{136} \text{ Mg/L}$$

$$= (10 + 10) \text{ Mg/L}$$

$$= 20 \text{ Mg/L}$$

$$\text{Total Hardness} = 15 + 20 = 35 \text{ Mg/L} = \text{ppm.}$$

SOFTENING METHODS



Water Softening :-

Removal of hardness of water whether temporary or permanent hardness is done through the process called softening of water. It is very essential process since hard water is unsuitable for domestic as well as industrial purposes, In steam generation hard water creates number of problems like scale and sludge formation, priming and foaming etc.

Hardness can be removed by two methods

- (1) External Treatment
- (2) Internal Treatment

Lime –Soda Process

This is the most important method of water softening.

PRINCIPLE :- The principle involved in this process the soluble calcium and magnesium salts in water are chemically converted into insoluble compounds, by adding calculated amount of **lime** [Ca(OH)_2] and **soda** [NaCO_3] . **Calcium carbonate** [CaCO_3] and **magnesium hydroxide** [Mg(OH)_2] , so precipitated, are filtered off.

Cold Lime –Soda Process

In this method-calculated amount of chemical (lime and soda) are mixed with water at room temperature. The precipitates formed are finely divided, so they do not settle down easily and can't be filtered easily. So it is essential to add small amounts of Coagulants (like alum, aluminum sulphate, sodium acuminate etc.). Which hydrolyze to flocculent (precipitate), gelatinous precipitate of aluminum hydroxide and entraps the fine precipitates.

Cold L-S process provides water, containing a residual hardness of 50 to 60 ppm.

- Raw water and calculated amount of chemicals (lime + soda + coagulant) are fed on top into the inner vertical circular chamber, fitted with a vertical rotating shaft varying a number of paddles.
- As the raw water and chemicals flow down, there is a vigorous stirring and continuous mixing, so softening of water takes place.
- The heavy sludge settles down in the outer chamber by the time and softened water reaches up.
- The softened water then passes through a filtering media to ensure complete removal of sludge.
- Filtered soft water finally flows out continuously through the outlet at the top.
- Sludge settings at the bottom of the outer chamber are drawn off occasionally.

Hot Lime –Soda Process

In this process water is treated with required chemicals at a temperature of 80 °C to 150 °C.

Hot L-S process provides water, containing a residual hardness of 15 –30 ppm. The softener consists of following three parts-

- (a) **Reaction Tank** – The tank has three separate inlets and third for superheated steam. After their entry they are mixed. The reaction starts and gets completed in the reaction tank.
- (b) **Conical Sedimentation Tank** – from reaction tank the reactants come in this tank and the sludge settles down.
- (c) **Sand filter** – It has a layer of lime and coarse sand, which works as a filter and makes it possible to completely remove the sludge from the softened water.

Processing -

- (i) In Hot L-S process reaction proceeds faster.
- (ii) No coagulants are needed because sludge and precipitates settle easily.
- (iii) Some dissolved gases like CO₂ also driven out of the water.
- (iv) Viscosity of softened water is lower, so filtration of water becomes much easier.
- (v) The softening capacity of hot process is many times higher than that of the cold process.

Advantages of Lime –soda Process.

- (i) Lime Soda process is very economical.
- (ii) It removes not only hardness causing salts but also minerals.
- (iii) Due to alkaline nature of treated water, pathogenic bacteria's in water are reduced.
- (iv) Iron and manganese are also removed.
- (v) Treated water is alkaline and therefore less corrosive.

Disadvantages of Lime –soda Process.

- (i) For efficient and economical softening, careful operation and skilled supervision is required.
- (ii) Disposal of large amounts of sludge poses a problem.
- (iii) This can remove hardness only up to 15 ppm, which is not good for boilers.

Calculation of Lime-Soda Requirement-

Constituent	Reaction	Need
Permanent Hardness of CaCl ₂ and CaSO ₄	$\text{CaCl}_2 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + 2\text{NaCl}$	S
	$\text{CaSO}_4 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + \text{Na}_2\text{SO}_4$	S
Perm. Hard. Of MgCl ₂ and MgSO ₄	$\text{MgCl}_2 + \text{Ca(OH)}_2 \rightarrow \text{Mg(OH)}_2 \downarrow + \text{CaCl}_2$	L + S
	$\text{CaCl}_2 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + 2\text{NaCl}$	
Ca(HCO ₃) ₂ (Temp. Ca)	$\text{Ca(HCO}_3)_2 + \text{Ca(OH)}_2 \rightarrow 2\text{CaCO}_3 \downarrow + 2\text{H}_2\text{O}$	L
Mg(HCO ₃) ₂ (Temp. Mg)	$\text{Mg(HCO}_3)_2 + 2\text{Ca(OH)}_2 \rightarrow 2\text{CaCO}_3 \downarrow + 2\text{H}_2\text{O}$	2L
HCO ₃ ⁻ (NaHCO ₃)	$2\text{HCO}_3^- + \text{Ca(OH)}_2 \rightarrow 2\text{CaCO}_3 \downarrow + \text{H}_2\text{O} + \text{CO}_3^{2-}$	L - S
	$\text{CO}_2 + \text{Ca(OH)}_2 \rightarrow \text{CaCO}_3 \downarrow + \text{H}_2\text{O}$	
Dissolved CO ₂		L
Free acids H ⁺ HCl and H ₂ SO ₄	$2\text{HCl} + \text{Ca(OH)}_2 \rightarrow \text{CaCl}_2 + 2\text{H}_2\text{O}$	L+S
	$\text{CaCl}_2 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + 2\text{NaCl}$	
H ₂ SO ₄	$\text{H}_2\text{SO}_4 + \text{Ca(OH)}_2 \rightarrow \text{CaSO}_4 + 2\text{H}_2\text{O}$	L+S
	$\text{CaSO}_4 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + \text{Na}_2\text{SO}_4$	
Coagulant FeSO ₄	$\text{FeSO}_4 + \text{Ca(OH)}_2 \rightarrow \text{Fe(OH)}_2 \downarrow + \text{CaSO}_4$	L+S
	$\text{CaSO}_4 + \text{Na}_2\text{CO}_3 \rightarrow \text{CaCO}_3 \downarrow + \text{Na}_2\text{SO}_4$	
Al ₂ (SO ₄) ₃	$2\text{Al}_2(\text{SO}_4)_3 + 3\text{Ca(OH)}_2 \rightarrow 2\text{Al(OH)}_3 \downarrow + 3\text{CaSO}_4$	L+S
	$3\text{CaSO}_4 + 3\text{Na}_2\text{CO}_3 \rightarrow 3\text{CaCO}_3 \downarrow + 6\text{Na}^+$	
NaAlO ₂	$\text{NaAlO}_2 + \text{H}_2\text{O} \rightarrow \text{Al(OH)}_3 \downarrow + \text{NaOH}$	-L

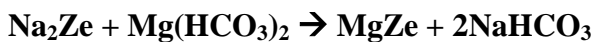
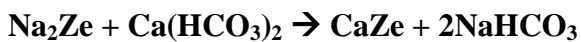
ZEOLITE OR PERMUTIT PROCESS

The word zeolite is derived from two Greek words (zein + lithos) means 'boiling stone'. Natural zeolites are non porous in nature. Chemical structure of sodium zeolite may be represented by $\text{Na}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot x \text{SiO}_2 \cdot Y \text{H}_2\text{O}$. Where $x = 2 - 10$, $Y = 2 - 6$.

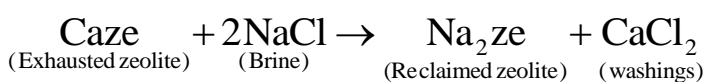
Zeolite is **hydrated sodium aluminosilicate**, capable of exchanging reversibly its sodium ions for hardness – producing ions in water. Zeolites are also known as permutits. Zeolites are of two types. –

- (i) Natural Zeolites
 - (ii) Synthetic zeolites.
- (i) Natural Zeolite – are non porous. Ex.
- Natrolite $\text{Na}_2\text{O}, \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2 \cdot 2\text{H}_2\text{O}$
- Thomsonite $(\text{Na}_2\text{O}, \text{CaO}) \cdot \text{Al}_2\text{O}_3 \cdot 2 \text{SiO}_2 \cdot 2 \frac{1}{2} \text{H}_2\text{O}$
- (ii) Synthetic Zeolite – They are porous and possess gel structure. Such zeolite passes higher exchange capacity than natural zeolite but they are less durable.

PROCESS :- Hard water is percolated at a specific rate through a bed of zeolite, kept in a cylinder. Hardness causing ions (Ca^{2+} , Mg^{2+} etc) are retained by the zeolite as CaZe and MgZe , while outgoing water contains sodium salts.



Regeneration:- When the zeolite bed is exhausted (saturated with Ca^{2+} and Mg^{2+}), it can be regenerated and reused. **Exhausted zeolite is reclaimed by treating the bed with a brine (10% NaCl) solution.**



The washings are led to drain and the regenerated zeolite bed thus – obtained is used again for softening purpose.

LIMITATION:-

- (i) Water with turbidity should not be used as pores of zeolite get clogged.
- (ii) PH of water should not be too high or too low as it affects zeolites.

- (iii) Water containing Fe^{2+} and Mn^{2+} ions should be avoided because Fe^{2+} will form their zeolite which can't be easily regenerated.
- (iv) Hot water can't be used as it dissolves zeolite.
- (v) Mineral acids, if present in water, destroy the zeolite bed.

ADVANTAGES

- (i) Hardness is completely removed.
- (ii) Equipment used is compact and occupies less space.
- (iii) There is no danger of sludge formation.
- (iv) It is quite clean.
- (v) It requires less time for softening.

ZEOLITE PROCESS	LIME SODA PROCESS
(i) Water with zero hardness is produced.	(i) Water with 15 to 50 pm hardness is produced.
(ii) Capital cost is higher.	(ii) Capital cost is lower.
(iii) Operation cost is lower because exhausted zeolite is regenerated.	(iii) Operation cost is higher because lime and soda are consumed.
(iv) Plant is compact and occupies less space.	(iv) Plant occupies more space.
(v) Can not be used for hot water, acidic water or turbid water.	(v) Process is free from any such limitations.
(vi) No. problem of sludge formation.	(vi) There may be problem after precipitation.
(vii) Salt causing temporary hardness are converted into NaHCO_3 which is present (i) soft water.	(vii) Temporary hardness is completely removed in the form of insoluble CaCO_3 and $\text{Mg}(\text{OH})_2$.
(viii) It does not involve any secondary operation like salt, lime, coagulation, filtration.	(viii) This involves all problems associated with setting coagulation and filtration.

Solved Examples Based on Hardness.

Ex. (1) The hardness of 1000 litres of a water sample was completely removed by a zeolite softener. The zeolite had required 30 litres of NaCl solution, containing 1,500 mg/L of NaCl for regeneration. Calculate the hardness of the water sample.

Solution-

30 litres of NaCl solution contains

$$= 1.50 \times 30 \text{ g} = 45 \text{ g of NaCl.}$$

$$= 45 \times \frac{50}{58.5} \text{ g of CaCO}_3 \text{ equivalent hardness.}$$

This much hardness may be deemed to be present in 1000 litres of water sample.

∴ Hardness of the water sample.

$$= 45 \times \frac{50}{58.5} \times \frac{1,000}{1,000} \text{ Mg/L}$$

$$= 38.46 \text{ ppm}$$

Ans.

Ex. (2) An exhausted zeolite softener was regenerated by passing 150 litres of NaCl solution, having a strength of 150 g/l of NaCl. How many litres of hard water sample, having hardness of 600 ppm can be softened, using softener ?

Solution-

150 litres of NaCl solution contains

$$150 \times 150 \text{ g} = 22,500 \text{ g NaCl}$$

$$= 22,500 \times \frac{50}{58.5} \text{ g of CaCO}_3 \text{ eq. hardness}$$

Given that 1 litre of hard water contains 600 ppm hardness = 600 mg of CaCO₃ = 0.6 g of CaCO₃.

∴ The amount of hard water that can be softened by this softener

$$= \frac{22,500 \times 50}{0.6 \times 58.5}$$

$$= 32,051 \text{ litres.}$$

Ex. (3) The hardness of 100000 litres of a sample of water was completely removed by passing it through a zeolite softener. The softener then required 400 litres of sodium chloride solution containing 100 g/litre of NaCl for regeneration. Calculate the hardness of the water sample.

Solution –

400 L of NaCl solution

$$= 400 \text{ L} \times 100 \text{ g/L} = 40,000 \text{ g NaCl}$$

$$= 40,000 \times \frac{50}{58.5} \text{ g CaCO}_3 \text{ eq.}$$

$$= 34,188 \text{ g CaCO}_3 \text{ eq.}$$

∴ Hardness of 100,000 L water = 34,188 g CaCO₃ eq.

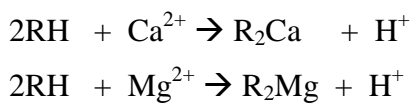
Or

$$\begin{aligned} \text{Hardness of 1L water} &= \frac{34,188}{100,000} \\ &= 0.3419 \text{ g CaCO}_3 \text{ eq.} \\ &= 341.9 \text{ mg} \end{aligned}$$

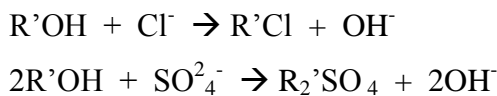
ION EXCHANGE OR DE-IONIZATION PROCESS:-

- Ion exchange resins are insoluble cross-linked, long chain organic polymers with a micro-porous structure and the 'functional groups' attached to the chains are responsible for the ion-exchanging properties.
- Resins containing acidic functional groups (-COOH, -SO₃H etc) are capable of exchanging their H⁺ ions with other cations.
- Resins containing basic functional groups (-NH₂) are capable of exchanging their anion with other anion.
- (i) **Cation exchange resins (RH⁺)** - are mainly styrene divinyl benzene copolymers, which on sulphonation or carboxylation become capable to exchange their hydrogen ions with the cations in the water.
- (ii) **Anion exchange resins (R' OH⁻)** are styrene – divinyl benzene or amine formaldehyde copolymers, which contain amino groups as an integral part of the resin. These after treatment with dil NaOH solution become capable to exchange their OH⁻ anions with other anions of water.

PROCESS :- The hard water is passed first through cation exchange column, which removes all the cations like Ca²⁺, Mg²⁺ etc. from it, and equivalent amount of H⁺ ions are released from this column to water. Thus;



After cation exchange column, the hard water is passed through anion exchange column, which removes all the anions like SO₄²⁻, Cl⁻ etc. present in the water and equivalent amount of OH⁻ ions are released from this column.



H⁺ and OH⁻ ions get combined to produce water molecule.



Thus, the water coming out from the exchanger is free from cations as well as anions. Ion free water, is known as deionized or de-mineralized water.

REGENERATION :-

After long use the exchange capacity of cation and anion exchange resins is lost, they are then called to be exhausted.

The exhausted cation exchange column is regenerated by passing a solution of **dil HCl** or **dil H₂SO₄**.



The exhausted anion exchange column is regenerated by passing a solution of dil NaOH.



Advantages :-

- (i) The process can be used to soften highly acidic or alkaline water.
- (ii) It produces water of very low hardness (~2ppm). So it is very good for treating water for use in high pressure boiler.

Disadvantages :-

- (i) The equipment is costly and more expensive chemicals are needed.
- (ii) If water contain turbidity, then the output of the process is reduced.

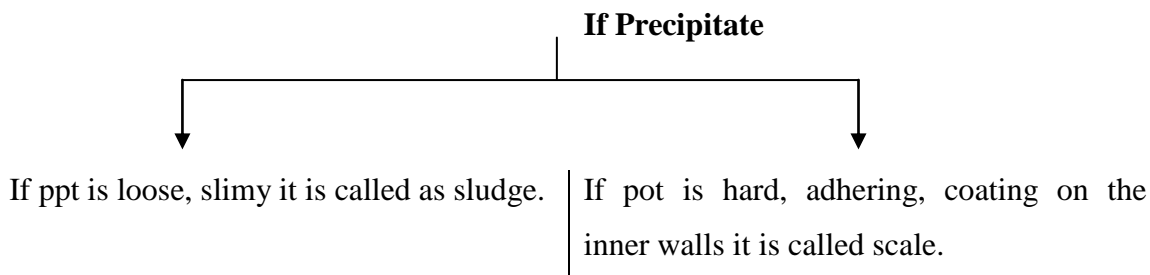
BOILER TROUBLE

A proper quality of water for use in boilers is very important. If impure water is made use of as boiler feed water, then following boiler problems may occurs.

- (i) **Sludge and scale formation.**
- (ii) **Corrosion of boiler metal.**
- (iii) **Caustic embrittlement.**
- (iv) **Priming and foaming.**

(i) Sludge and Scale Formation.

In boilers, water evaporates continuously and the concentration of the dissolved salts increase progressively. When their concentrations reach saturation point, they are thrown out of water in the form of precipitates on the inner walls of the boiler.



Sludge :-

- (1) It is a soft, loose, slimy precipitate.
- (2) It can be easily scrapped off with a wire brush.
- (3) Sledges are formed by substances which have greater solubility in hot water than in cold water.
Ex. MgCO₃, MgCl₂, MgSO₄, etc.
- (4) It is formed at colder portions of the boiler and collects in areas, where flow rate is slow.

Disadvantages of Sludge formation :-

- (1) Sludge is poor conductors of heat, so they tend to waste a portion of heat and thus decrease boiler efficiency.
- (2) If sludge are formed along with scale, then sludge gets entrapped in the scale and both get deposited as scale.
- (3) Excessive sludge formation disturbs the working of the boiler.
- (4) Sludge deposited on pipe connection, plug opening so choking of pipes takes place.

Prevention of sludge formation:-

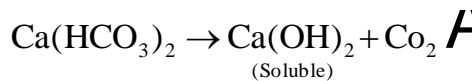
- (1) By using well softened water.
- (2) By frequent 'Blow down operation'
Blow down operation is "Partial removal of concentrated water through a outlet at the bottom."

SCALE :-

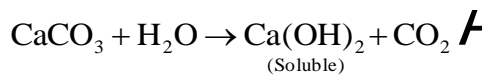
- (1) Scales are hard deposit.
- (2) They stick very firmly to the inner surface of the boiler.
- (3) They are difficult to remove, even with the help of hammer and chisel.
- (4) Scales are main source of boiler trouble.

Formation of Scale due to –

- (1) **Decomposition of Calcium bicarbonate-**



This scale is soft and is the main cause of scale in lower pressure boiler. But in high pressure boilers CaCO_3 is soluble.

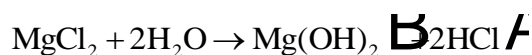


- (2) **Deposition of CaSO_4** – The solubility of CaSO_4 in water decreases with rise of temperature.

Temp.	15°C	230°C	320°C
Solubility	3,200 ppm	55 ppm	27 ppm.

Means CaSO_4 is soluble in cold water but almost completely insoluble in super heated water.

- (3) **Hydrolysis of Mg Salts-**



It forms $\text{Mg}(\text{OH})_2$ ppt. This forms a soft type of scale.

- (4) **Presence of silica – (SiO₂)** – Even present in small quantities deposits as MgSiO₃ and CaSiO₃. It is deposited in the inner walls of boiler and very difficult to remove.

Disadvantage of Scale formation-

- (1) **Wastage of fuel** – Scales are poor conductor of heat from boiler to inside water is decreased. So excessive or over heating is needed, this causes increase in fuel consumption.

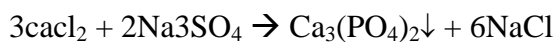
Thickness of Scale	0.325	0.625	1.25	2.5	12
Wastage of fuel	10%	15%	50%	80%	150%

- (2) **Lowering of boiler safety** – The over heating of the boiler tube makes the boiler material softer and weaker this causes distortion of boiler tube and make boiler unsafe.
- (3) **Decrease in efficiency** – Scales sometimes deposited in the valves and condensers of the boiler and choke them, this results in decrease in efficiency.

Prevention of Scale formation-

Internal treatment – An internal treatment is accomplished by adding a proper chemical to the boiler water. Some methods are-

- (1) **Colloidal Conditioning** – In lower pressure boiler by adding organic substance like – kerosene, tannin, agar – agar. Scale formation can be avoided. They get converted over the scale, so scale will be non sticky and loose deposits, which can easily be removed by blow down operation.
- (2) **Phosphate Conditioning** – In high pressure boilers by adding sodium phosphate scale formation can be avoided. They formed non-adherent and easily removable, soft sludge of phosphate. Which can easily removed by blow – down operation.



- (i) NaH₂PO₄ - Sodium dihydrogen phosphate (acidic)
- (ii) Na₂HPO₄ - Disodium hydrogen phosphate (weak alkaliz)
- (iii) Na₃PO₄ - Tri sodium phosphate (alkaline)

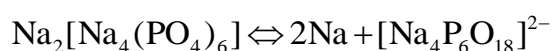
The use of salt depends upon the alkalinity of water. Calcium precipitated at PH value b/w 9.5 – 10.5.

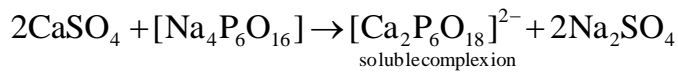
- (3) **Carbonate Conditioning** – In lower pressure boiler scale formation can be avoided by adding sodium carbonate.



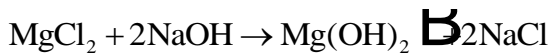
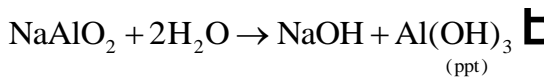
CaCO₃ is loose sludge which can be removed by blow down operation.

- (4) **Calgon Conditioning** – By adding calgon (Sodium hexa meta phosphate (Na₆PO₃)₆) in boiler water. It forms soluble complex with Ca⁺ ion.





(5) **Treatment with sodium aluminate (NaAlO₂)** :- NaAlO₂ gets hydrolysed yielding NaOH and a gelatinous precipitate of aluminum hydroxide.

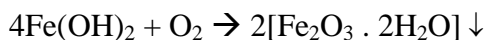
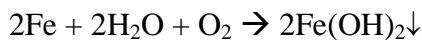


The ppt of Mg(OH)₂ plus Al(OH)₃ produced inside the boiler, entraps finely suspended and colloidal impurities, including oil drops and silica.

(ii) CORROSION OF BOILER METAL

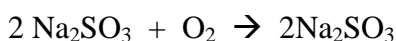
Boiler corrosion is decay of boiler material by a chemical attack by its environment. Main reasons for boiler corrosion are-

(a) **Dissolved Oxygen** – Water usually contains above 8 mL of dissolved oxygen per litre. Dissolved oxygen in presence of high temperature, attacks boiler material-

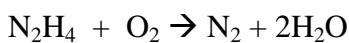


Rust.

Removal of dissolved Oxygen-



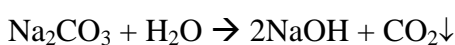
so, sulphite



(b) **By Mechanical de aeration** – Water spraying in a perforated plate – fitted tower, heated from sides and connected to vacuum pump. High temperature low pressure and large exposed surface reduces the dissolved oxygen in water.

(iii) CAUSTIC EMBRITTLEMENT

This type of boiler corrosion is caused because of use of high alkaline water in high pressure boilers. When water is softened by lime and soda process and is fed into the boiler it may be likely that some residual Na₂CO₃ is still present in the softened water. Na₂CO₃ decomposes to give NaOH and CO₂, and NaOH thus produced makes the boiler water caustic.



The NaOH containing water flows into the minute hair cracks always present in the inner side of boiler by capillary action. Here water evaporates and the dissolved caustic soda concentration increases progressively and attacks the surrounding boiler material and iron is dissolved as sodium ferrate. This causes embrittlement of boiler walls more particularly stressed parts. Like bends, joints rivets etc. causing even boiler failure.

Embrittlement arises due to setting up of a concentration cell, with the iron surrounded by dil NaOH acts as a cathode while the iron surrounded by conc. NaOH acting as the Anode.

Iron at + rivets, bends Joints, etc.	Concentrated NaOH Solution	Dilute NaOH Solution	- Iron at Plane surfaces.
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Caustic Embrittlement can be avoided.

- (i) By using sodium phosphate as softening reagent instead of sodium carbonate.
- (ii) By adding tannin or lignin to boiler water, since these blocks the hair cracks.
- (iii) By adding sodium sulphate the boiler water;

It has been observed that caustic cracking can be prevented, if Na₂SO₄ is added to boiler water so that the ratio-

$$\frac{\text{Na}_2\text{SO}_4 \text{ concentration}}{\text{NaOH concentration}}$$

Is kept as 1 : 1 : 2 : 1 and 3 : 1 in boilers working respectively at pressure up to 10,20 and above 20 atmosphere.

(iv) PRIMING AND FOAMING

PRIMING – When steam is generated rapidly in the boilers, some droplets of the liquid water are carried along with the steam. This process is called wet steaming or priming.

Priming is caused by-

- (i) The presence of large amount of dissolved solids.
- (ii) High steam velocities.
- (iii) Sudden boiling.
- (iv) Improper boiler design.
- (v) Sudden increase in steam production rate.

Priming can be avoided by-

- (i) Avoiding rapid change in steaming rate.
- (ii) Proper boiler design so that water level in boilers may be maintained at low level.

- (iii) Only soft water to be used.

FOAMING – Foaming is the formation of small but stable bubbles above the surface of water, which do not break easily.

Foam formation takes place when concentration of solids in the surface layer is different from that in the mass of the liquid.

Foaming is caused by – The presence of substances like oil (which greatly reduce the surface tension of water.)

Foaming can be avoided By-

- (i) The addition of antifoaming agents which reduces the surface tension of water. Ex.- castor oil.
- (ii) Removing oil from boiler water by adding compound like sodium aluminate.

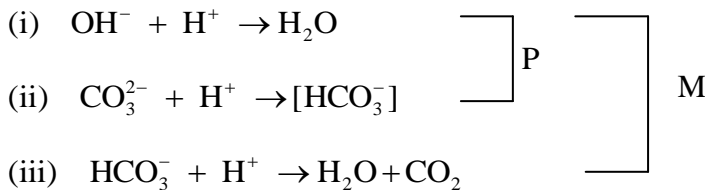
Determinate of Alkalinity-

Alkalinity of water means the total content of those substances in it, which causes an increased $[OH]^-$ upon dissociation.

Alkalinity of water may be due to presence of:

- (i) Caustic alkalinity (due to OH^- and due CO_3^{2-} ions)
- (ii) Temporary hardness (due to HCO_3^-)

These can be estimated separately by titration against standard acid, using phenolphthalein and methyl orange as indicator. The determinations are based on following reaction.



The titration of the water sample against a standard acid up to phenolphthalein end point (P) marks the completion of reaction, (i) and (ii) only this amount of acid used thus corresponds to hydroxide plus 1/2 of normal carbonate present.

On the other hand, titration of water sample against a standard acid to methyl orange end point (M) marks the completion of reaction (i), (ii) and (iii). Hence the total amount of acid used represent the total alkalinity.

Thus

$$P = OH^- \text{ and } \frac{1}{2}CO_3^{2-}$$

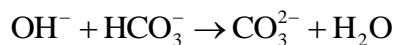
$$M = OH^-, CO_3^{2-} \text{ and } HCO_3^-$$

The possible combinations of ions causing alkalinity

- (i) water are-

(ii) OH^- Only or (ii) CO_3^{2-} only or (iii) HCO_3^- only or (iv) OH^- and CO_3^{2-} together (v) CO_3^{2-} and HCO_3^- together.

* The possibility of OH^- and HCO_3^- ions together is ruled out because they combine instantaneously to form CO_3^{2-} ions.



thus, OH^- and HCO_3^- ions can't exist together in water. On the basis of same, all the three (OH^- , CO_3^{2-} and HCO_3^-) can't exist together.

→ Table is as follows.

Alkalinity	OH^-	CO_3^{2-}	HCO_3^-
P=0	Nil	Nil	M
P=M	M	Nil	Nil
P= 1/2 M	Nil	2P	Nil
P> 1/2 M	(2P-M)	2(M-P)	Nil
P < 1/2 M	Nil	2P	[M-2P]

Alkalinity is generally represented in ppm.

Nu. → 100 ml of water sample, on titration with N/50 H_2SO_4 gave a titre value of 5.8 ml to [P] end point and 11.6 ml to [M] end point. Calculate the alkalinity of the water sample in terms of CaCO_3 and comment on the type of alkalinity present.

Solⁿ → P = 5.8 ml, M = 11.6 ml

Since P = 1/2 M, it means all alkalinity is due to CO_3^{2-} only.

Further, the volume of N/50 H_2SO_4 eq. To CO_3^{2-} present in 100 ml of water sample.

$$= 2P$$

$$= 2 \times 5.8 = 11.6 \text{ ml}$$

Since 1 ml of 1N H_2SO_4 = 50 mg of CaCO_3

$$11.6 \text{ ml of N/50 } \text{H}_2\text{SO}_4 = 50 \times 11.6 \times (\text{N/50})$$

$$= 11.6 \text{ mg of } \text{CaCO}_3$$

This is the CO_3^{2-} present om 100 ml of water

∴ Amount of CO_3^{2-} present in 1 litre of water

$$= 11.6 \times (1000/100)$$

$$= 116 \text{ mg/L} = 116 \text{ ppm}$$

Result = The alkalinity of water sample is 116 ppm which is only due to CO_3^{2-} .

Nu. (2) A water sample is not alkaline to [P] However, 100 ml of the sample, on titration with N/50 HCl, required 16.9 ml to obtain the end point, using [M] as indicator, are the types and amount of alkalinity present in the sample ?